## PROPOSED INTEGRATED HEALTH \& EDUCATION PRECINCT DESIGNATION

## 58-68 DELANCEY STREET, ORMISTON

Traffic Impact Assessment
For 'The Hub Precinct Pty Ltd'

## Table of Contents

1. INTRODUCTION .....  4
2. CONTEXT OF THE DEVELOPMENT SITE ..... 5
2.1 DEVELOPMENT SITE ..... 5
2.2 EXISTING ROAD NETWORK .....  6
3. DETAILS OF THE PROPOSED DEVELOPMENT ..... 9
3.1 PROPOSED DEVELOPMENT .....  9
3.2 ACCESS ARRANGEMENTS ..... 10
3.3 LIMITED ACCESS POLICY ..... 11
4. IMPACT ASSESSMENT ..... 12
4.1 BACKGROUND TRAFFIC ..... 12
4.2 IMPACT ASSESSMENT AREA ..... 12
4.3 TRIP GENERATION ..... 13
4.4 TRIP DISTRIBUTION ..... 14
4.5 DEVELOPMENT TRAFFIC ..... 14
4.6 DESIGN TRAFFIC ..... 14
4.7 IMPACT ASSESSMENT BASED ON MICROSIM MODELLING ..... 14
4.8 ACCESS ARRANGEMENTS - IMPACT ASSESSMENT ..... 17
5. SUMMARY ..... 22
APPENDIX A - SITE PLANS ..... 23
APPENDIX B- RAW TRAFFIC SURVEY DATA ..... 24
APPENDIX C- TRAFFIC MOVEMENT DIAGRAMS ..... 25
APPENDIX D- MICRO SIMLUATION MODELLING REPORT ..... 26
APPENDIX E- SIDRA OUTPUTS ..... 27
APPENDIX F- CONCEPT INTERSECTION DESIGNS ..... 28

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## 1. INTRODUCTION

Lambert \& Rehbein (SEQ) Pty Ltd has been commissioned by The Hub Precinct Pty Ltd to undertake a Traffic Impact Assessment for a proposed mixed use commercial development located at 58-68 Delancey Street, Ormiston QLD 4160, which is formally described as 0/SP308738, 0-2/SP308739; 0/SP308740; 4/SP308740; and $10-16 /$ SP314782. The development site currently contains existing and approved medical and education buildings, a car park, and a portion of vacant land, with a total site area of approximately 5.2ha.
The proposed designation is for an Integrated Health \& Education Precinct, consisting of a private hospital, medical consulting suites, research and education facility, residential aged care, and ancillary retail." This report has considered the sites full development potential which also includes childcare, independent living and a community hub which will be assessed at a future date via the DA process. It is understood that the development will be completed over three (3) stages. The proposed development proposes to gain access to the external road network via a new signalised intersection on Finucane Road and an existing access on Delancey Street. The proposed site layout, prepared by Destravis Group, is attached in Appendix A.
The development application is being pursued through the Ministerial Designation process and this traffic assessment forms part of the application material. We note that a previous detailed traffic assessment had been undertaken focussing on the proposed access to Finucane Road and was documented in a Lambert \& Rehbein Technical Note (B19590TN002 Rev C) dated 10/11/2021. The intent of this initial separate engagement was to review the proposed new site access and demonstrate that a signalised intersection could be implemented in this location without significant implication for safety and efficiency of the state-controlled road network.

Subsequent to this previous work we have undertaken further detailed traffic analysis with a more networkbased traffic analysis that has been undertaken in accordance with the requirements of the GTIA. This report documents the work undertaken and the findings and recommendations.

The site will be referred to as the 'development site' from hereon in.
This report has been undertaken to assess the potential impact that the proposed development could have on the external road network surrounding the site, and is set out as follows:

Section 2 discusses the existing land use and traffic arrangements in the vicinity of the proposed development site.

Section 3 provides details of the proposed development site, including an assessment of the site layout and access arrangements.

Section 4 displays the calculations and assumptions used to establish the forecast generation and distribution of the proposed development traffic including a network aggregate delay assessment based on Microsim Modelling.

Section 5 summarises the key outcomes of the traffic investigations.
Lambert \& Rehbein has derived the data in this report primarily from the data provided by the Client, and a desktop site investigation.

This report has been prepared on behalf of and for the exclusive use of the Client, and is subject to and issued in connection with the provisions of the agreement between Lambert \& Rehbein and the Client. Lambert \& Rehbein accepts no liability or responsibility whatsoever for or in respect of any use of or reliance upon this report by any third party.

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## 2. CONTEXT OF THE DEVELOPMENT SITE

This section of the report describes the context of the proposed development and includes a description of the existing road network, adjacent land uses, and existing public transport facilities servicing the site.

### 2.1 DEVELOPMENT SITE

The development site is located at 58-68 Delancey Street, Ormiston QLD 4160, which is formally described as 0/SP308738, 0-2/SP308739; 0/SP308740; 4/SP308740; and 10-16/SP314782. The development site currently contains existing and approved medical and education buildings, a car park, and a portion of vacant land, with a total site area of approximately 5.2ha.

The development site is zoned partially as 'Low Impact Industry' and partially 'Recreation and Open Space' as per the Redlands City Council Planning Scheme. The development site is generally surrounded by 'Low Density residential' developments to the north, 'Community Facilities' to the south and 'Medium Density residential' and 'neighbourhood centre' developments to the east. The development site in the context of the external road network is shown in Figure 2-1. The subject site has southern frontage to Finucane Road and eastern frontage to Delancey Street. There are no other road frontages from which can gain access.


Figure 2-1 Proposed Development Site

### 2.2 EXISTING ROAD NETWORK

Inspection of the land use, road condition, intersection characteristics, public transport facilities, pedestrian access, and cyclist provisions surrounding the proposed development site has been undertaken in preparation of this assessment. This was completed to collect information about the road network operation, safety characteristics, public transport network and specific network / land-use factors potentially of influence to the proposed development.

### 2.2.1 FINUCANE ROAD

Finucane Road runs along the southern frontage of the development site. Finucane Road is gazetted as a 'State Controlled Road' under the jurisdiction of the Department of Transport and Main Roads (DTMR). Additionally, we note that this section of Finucane Road at the site frontage is gazetted as a 'Limited Access Road' (LAR 2) and has a defined limited access policy. This is discussed further in Section 3 following.

The general form of Finucane Road is shown in Figure 2-2 and was observed to have the following characteristics at the site frontage:

- Two-way, four-lane, median divided road;
- Kerb and channel exist on the eastbound side of the road (approx. 260m along the site frontage);
- Carriageway width of approximately 16.22 m (including approx. 2 m median) at the site frontage;
- Finucane Road meets Delancey Street at a four-way signalised intersection, more details in Section 2.2.3;
- No parking permitted on either side of the road;
- Pedestrian footpaths provided on the eastbound side of the road along the site frontage; and
- Posted speed limit of $70 \mathrm{~km} / \mathrm{hr}$.


Figure 2-2 Finucane Road (Facing west)

### 2.2.2 DELANCEY STREET

Delancey Street is located on the eastern frontage of the development site. Delancey Street is gazetted as a 'local road' as per Redlands City Council Planning Scheme. The general form of Delancey Street is shown in Figure 2-3 and was observed to have the following characteristics at the site frontage:

- Two-way, two-lane, median divided road;
- Kerb and channel exist on both sides of the road;
- Carriageway width of approximately 17.6 m (including median and turn lanes as can been seen in Figure 2-3) at the site frontage;
- Delancey Street meets Finucane Road at a four-way signalised intersection, more details in Section 2.2.3;
- Shoulder parking permitted on both sides of the road;
- Pedestrian footpaths provided on both sides of the road; and
- Posted speed limit of $50 \mathrm{~km} / \mathrm{hr}$.


Figure 2-3 Delancey Street (Facing North)

### 2.2.3 DELANCEY STREET / FINUCANE ROAD SIGNALISED INTERSECTION

The Delancey Street / Finucane Road signalised intersection is an existing four-way signalised intersection located at the south-eastern corner of the development site. The existing intersection layout is as demonstrated in the aerial imagery provided in Figure 2-4. It should be noted that as a result of the proposal, the Delancey Street / Finucane Road signalised intersection will be upgraded. More details are provided in Section 4 regarding the proposed upgrades.


Figure 2-4 Existing Delancey Street / Finucane Road Signalised Intersection

## 3. DETAILS OF THE PROPOSED DEVELOPMENT

This section of the report describes the nature of the proposed development, the proposed access arrangements, servicing arrangements and on-site manoeuvrability.

### 3.1 PROPOSED DEVELOPMENT

The proposed designation is for an Integrated Health \& Education Precinct, consisting of a private hospital, medical consulting suites, research and education facility, residential aged care, and ancillary retail." This report has considered the sites full development potential which also includes childcare, independent living and a community hub which will be assessed at a future date via the DA process. It is understood that the development will be completed over three (3) stages.

The proposed site layout and detailed functional plans, prepared by Destravis Group, are attached in Appendix A. We note that these planning layouts have evolved as design of the site has developed and further details of the site gradings and conceptual engineering design has also evolved. As such the current broad land uses have changed as the site constraints have become known.
A summary of the proposed yields as currently proposed are summarised in Table 3-2.

Table 3-1 Proposed Development Yields

| USE |  |  |
| :---: | :---: | :---: |
| PRIVATE HOSPITAL | 148 Beds + 14 Theatres | $22,411 \mathrm{~m}^{2}$ GFA |
| DAY SURGERY | 18 Day Beds (inc. within the Private Hospital) |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | - | 4,614 m² GFA |
| CHILD CARE | 150 Places | 1,200 m² GFA |
| SPECIAL RETAIL | - | 6,213 m² GFA |
| RESEARCH INSTITUTE | - | 4,407 m² GFA |
| ASSISTED LIVING UNIT \& FACILITIES | 200 Units + Facilities | 25,000 m² GFA |
| COMMUNITY HUB | - | 2,000 m² GFA |
| AGED CARE | 80 Beds + Ancillary Area | 6,756 m² GFA |
| TOTAL |  | 72,601 m² GFA |

We note that traffic modelling undertaken for the project has included detailed SIDRA intersection analysis and detailed microsimulation modelling utilising the Aimsun modelling package (see Section 4 of this report). The modelling work undertaken was significant and was based on a previous land use scheme that had estimated a higher development yield that the current proposal. This relates to the areas and number of beds adopted for the Aged Care Facility. The yield adopted in the traffic modelling is shown in Table 3-2 below and clearly represents a higher development yield and as such a higher level of traffic generation.

On this basis we have not provide new traffic modelling scenarios as the modelling undertaken will inherently include safety margins due to the higher traffic generation rates.

Table 3-2 Proposed Development Yields

| USE |  |  |
| :---: | :---: | :---: |
| PRIVATE HOSPITAL | 148 Beds + 14 Theatres | 22,411 $\mathrm{m}^{2}$ GFA |
| DAY SURGERY | 18 Day Beds |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | - | 4,614 m² GFA |
| CHILD CARE | 150 Places | 1,200 m² GFA |
| SPECIAL RETAIL | - | 6,213 m² GFA |
| RESEARCH INSTITUTE | - | 4,407 m² GFA |
| ASSISTED LIVING UNIT \& FACILITIES | 200 Units + Facilities | 25,000 m² GFA |
| COMMUNITY HUB | - | 2,000 m² GFA |
| AGED CARE | 134 Beds + Ancillary Area | 11,163 m² GFA |
| TOTAL |  | 77,008 $\mathrm{m}^{2}$ GFA |

### 3.2 ACCESS ARRANGEMENTS

The proposed development will gain access to the external network via a new signalised intersection on Finucane Road. Finucane Road is gazetted a State Controlled Road and a Limited Access Road along the site frontage.

The development site has an existing priority-controlled, all-movement access provided on Delancey Street, which is designated a local road as per the Redlands City Council. For a development of the nature proposed, it is not considered viable from a traffic engineering perspective to have this access as the sole access into the proposed development. This would lead to safety concerns due to delay and general congestion on Delancey Street and the consequential impacts on the state-controlled road network as drivers becoming impatient. There is additionally limited opportunity to "significantly" upgrade the existing site access on Delancey Street given the constraints associated with land ownership and intersection proximity. It should be noted that as a result of the proposed development, the Delancey Street Access will be upgraded to ban right turns out of the site and to include a 20 m left turn lane into the site. A SIDRA intersection analysis of the Delancey Street Access intersection has been completed and has been included in Section 4.
The proposed signalised access intersection on Finucane Road will operate efficiently whilst also preserving the functionality, safety and efficiency of the state-controlled road. The intersection design will also ensure vulnerable users such as cyclists and pedestrians are accommodated and protected through the design of this access. A SIDRA intersection analysis of the proposed Finucane Road intersection has been completed and has been included in Section 4.

As part of the current conceptual designs, bicycle lanes have been provided on both sides of Finucane Road, and signalised pedestrians crossings have been provided across the site access and the Finucane Road eastern approach. We note that a signalised pedestrian crossing has not been provided on the Finucane Road western approach given there will likely be no pedestrian demand at this location.

The Concept Design for the site access intersection is shown in the plans prepared by Mortons Urban Solutions which have been informed by the detailed traffic modelling work undertaken as part of this project and as described in Section 4 following. The concept design of the intersection is included in Drawing No. 37801-XWP-005 Amend. A and included in Appendix F of this report.

### 3.3 LIMITED ACCESS POLICY

As discussed during pre-lodgement meetings with the SARA / DTMR, we note that Finucane Road along the site frontage is a limited access road (LAR 2) and as such the intent of the limited access policy requires consideration and assessment. We note that the current SDAP outlines that access to a road classified as a LAR 2 road can be considered subject to assessment

Further detailed traffic analysis has been completed and documented further in this traffic report and clearly shows that operationally the proposed access intersection is adequate from an operational perspective for a notional 10 year design horizon

The new intersection will provide approximately 370 m of spacing to the signalised intersection of Finucane Road and Delancey Street which we note is slightly short of the 400 m spacing requirement outlined in the Limited Access Policy albeit that we are of the view that the intent is achieved. It is important to note that the location of the proposed signalised intersection has been moved as far west along the site frontage as is physically possible. The location is constrained by the environmental corridor along the western side of the land and the existing bridge structure on Finucane Road.

We note that the proposed turn lanes have been reduced to ensure that the proposed access will not interfere on the ability for the adjacent intersection to be upgraded and that the intersection can be designed to meet the safety and design criteria set out in the Road Planning and Design Manual and/ or Austroads Guides, as per the Limited Access Policy.

## 4. IMPACT ASSESSMENT

This section provides details of the potential impact that the development traffic could have on the operation of the existing site access and the proposed new site access intersection. In particular, the assessment has focused on the existing Delancey Street priority-controlled access intersection at the north-eastern corner of the site, as well as proposed signalised access intersection on Finucane Road at the southern site boundary.

In addition, we have undertaken a detailed microsimulation modelling exercise, utilising the Aimsun modelling package, for the purposes of assessing the net delays impacts of the proposal on the external road network in accordance with the GTIA principles. This is discussed in more detail in Section 4.7 following.

### 4.1 BACKGROUND TRAFFIC

Vehicle movement survey data was collected at the following intersections on $29^{\text {th }}$ March 2022:

- Finucane Road / McDonald Road;
- Finucane Road / Dawson Road;
- Finucane Road / Delancey Street;
- Finucane Road / Wellington Street;
- Wellington Street / Russell Street;
- Wellington Street / Freeth Street; and
- Delancey Street / Freeth Street;

Vehicle movement data for the traffic moving in and out of the existing Delancey Street Access was collected on Thursday 29 October 2020. The through volumes utilised for this intersection were carried from the 2022 counts from the intersections to the north and south.

The intersection count data was collected from 6:00 AM to 9:00 AM and 2:30 PM to 6:30 PM, presented in 15minute periods to capture peak periods.

The AM and PM peak hours for the intersections were found to be as follows:

- AM: 7:45 AM to 8:45 AM; and
- PM: 4:00 PM to 5:00 PM.

Summary of traffic survey data is displayed in Figure C1 attached in Appendix C, with detailed traffic survey data included in Appendix B.

The opening year for the development is proposed to be 2024. To assess the future background traffic a linear growth rate of $1 \%$ per annum has been applied to all movements along Finucane Road and Delancey Street. It should be noted that the background traffic entering and exiting the existing site have not been grown. The predicted background traffic in 2024 and 2034 (10-year design horizon) has been presented in Figure C2 and Figure C3 attached in Appendix C.

### 4.2 IMPACT ASSESSMENT AREA

The impact assessment area that has been included in the network based Aimsun micro-simulation model, which is attached in Appendix $\mathbf{D}$, is as illustrated in Figure 4-1. It should be noted that this micro-simulation traffic model includes the proposed Finucane Road Site Access Intersection.


Figure 4-1 Impact Assessment Area

### 4.3 TRIP GENERATION

Additional traffic associated with the proposed development has been forecasted, using industry accepted peak hour traffic generation rates, from the RMS (formally RTA) Guide to Traffic Generating Developments and The Department of Transport and Main Roads (DTMR) Open Source Data, for development land uses. The traffic generation rates and in/out directionality of movements adopted for the analysis within this assessment, are shown in Table 4-1. For the purposes of this assessment, the speciality retail AM trip generation rate has been taken as $50 \%$ of the PM trip generation. The community hub has also been assumed to be ancillary to the development and will not generate individual trips external to the site.

Table 4-1 Generation \& Directionality Rates

| LAND USE | GENERATION RATE |  | DIRECTIONALITY (\% IN / \% OUT) |  | SOURCE |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak | PM Peak | AM Peak | PM Peak |  |
| PRIVATE HOSPITAL | $\begin{aligned} & -22.07 \text { trips }+1.04 \text { trips } x \\ & \text { beds } \end{aligned}$ | -22.07 trips +1.04 trips x beds | 50\% in / 50\% out | 50\% in / 50\% out | RMS (formally RTA) |
| DAY SURGERY |  |  |  |  |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | 9.81 trips / 100m² GFA | $\begin{aligned} & 5.80 \text { trips / } 100 \mathrm{~m}^{2} \\ & \text { GFA } \end{aligned}$ | 50\% in / 50\% out | 50\% in / 50\% out | DTMR Open Source Data |
| CHILD CARE | 0.8 trips / child | 0.7 trips / child | 50\% in / 50\% out | 50\% in / 50\% out | RMS (formally RTA) |
| SPECIAL RETAIL | 2.8 trips / $100 \mathrm{~m}^{2}$ GFA | 5.6 trips / 100m² GFA | $50 \%$ in / 50\% out | $50 \%$ in / 50\% out | RMS (formally RTA) |
| RESEARCH INSTITUTE | 2 trips / 100m² GFA | 2 trips / 100m² GFA | 90\% in / 10\% out | 10\% in / 90\% out | RMS (formally RTA) |
| ASSISTED LIVING UNIT \& FACILITIES | 0.2 trips per dwelling | 0.2 trips per dwelling | 80\% in / 20\% out | 20\% in / 80\% out | RMS (formally RTA) |
| AGED CARE | 0.2 trips per dwelling | 0.2 trips per dwelling | 80\% in / 20\% out | 20\% in / 80\% out | RMS (formally RTA) |
| COMMUNITY HUB | - | - | - | - |  |

Due to the nature of the site containing various mixed uses, it is expected that there will be cases of drivers visiting more than one (1) use during the same trip. These trips represent the likely cross-utilisation of the site and described as 'linked trips', they generally result in a reduction of trips to and from the site. A 10\% reduction has been assumed for the overall trips generated by the development site which will provide a reasonable forecast of potential traffic demands. As such, based on the above guidelines and assumptions, the estimated traffic generated by the proposed development is documented in Table 4-2.

Table 4-2 Development Traffic Generation

| LAND USE | YIELD | AM(IN) | AM (OUT) | PM (IN) | PM (OUT) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PRIVATE HOSPITAL | 148 BEDS + 14 THEATRES |  |  |  |  |
| DAY SURGERY | 18 Day Beds |  |  |  |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | 4,614 m ${ }^{2}$ GFA | 226 | 226 | 134 | 134 |
| CHILD CARE | 150 PLACES | 60 | 60 | 53 | 53 |
| SPECIAL RETAIL | 6,213 m ${ }^{2}$ GFA | 87 | 87 | 174 | 174 |
| RESEARCH INSTITUTE | 4,407 m ${ }^{2}$ GFA | 79 | 9 | 9 | 79 |
| ASSISTED LIVING UNIT \& FACILITIES | 200 UNITS + FACILITIES | 32 | 8 | 8 | 32 |
| AGED CARE | 134 BEDS + Ancillary Area | 21 | 5 | 5 | 21 |
| COMMUNITY HUB | 2,000 m ${ }^{2}$ GFA | - | - | - | - |
| Total Trips per Peak (10\% Cross-Utilisation) |  | 524 | 424 | 412 | 512 |

As illustrated in Table 4-2, the proposed development is anticipated to generate approximately 948 trips during AM peak and 924 trips during the PM peak.

### 4.4 TRIP DISTRIBUTION

The trip distribution adopted within the model is $77 \%: 23 \%$ split between the Finucane Road and Delancey Street accesses. The SIDRA intersection assessment adopted the distribution of traffic through the network that was an output from the Aimsun Micro-simulation Model, which has been included in Appendix D noting the availability of various route choices through the network.

### 4.5 DEVELOPMENT TRAFFIC

Based on the trip distribution outlined in Section 4.4, the trip generation for the development is displayed in Figure C4, attached in Appendix C.

It should be noted that due to the proposed upgrades, traffic movements through the network have altered including alterations to the "background" traffic. Where there are multiple routes available, and the proposal includes upgrades to address existing network constraints, it is routine that there will be some diversion of traffic as a result of improvements made to suit other network movement options. It is this diversion of traffic through the network as a result of the proposed upgrades that has resulted in the negative volumes on turning movements within the network.

### 4.6 DESIGN TRAFFIC

The design traffic scenarios (background traffic plus the development generated traffic) in 2024 and 2034, are displayed in Figure C6 and Figure C7, respectively attached in Appendix C.

### 4.7 IMPACT ASSESSMENT BASED ON MICROSIM MODELLING

Due to the volume of traffic that the proposed development site is anticipated to generate in the peak hours, the proposed development traffic was assessed in relation to the potential for it to impact over a broader area along the state-controlled and council-controlled road networks. The extent of the potential impacts included a broader "network" of road where various route choices were available which. As such, an assessment of the existing road network, including all stages of the development, was completed to analyse the operational impacts on the surrounding road network based on Aimsun Micro-simulation as opposed to relying solely on SIDRA based analysis. The micro-simulation model has been built with the existing (2022) surrounding road network traffic demand, as outlined in Section 4.1. The micro-simulation modelling report prepared by Adanner Pty Ltd has been attached in Appendix D.

The micro-simulation model has applied the background traffic (growth rate=1\%), trip generation, trip distribution, development traffic and design traffic highlighted above in Section 4.2, Section. 4.3, Section 4.4 and Section 4.5.
As part of the modelling of the development impacts the Aimsun micro-simulation model has been utilised to test with and without development scenarios along with the testing of various road network improvements that were being contemplated. This allowed the project team to identify the most effective mitigation strategies that would deliver the maximum benefit to the existing road users and would mitigate the impacts of the development and the new signalised intersection proposed on Finucane Road. The vehicle delay assessments were based on the microsimulation modelled outputs and importantly, the methodology associated with the delay assessment appropriately dealt with the redirected "background traffic" applying the "with development" network delays for the "base case" and "upgraded" networks to the background traffic only. This was done by essentially applying different vehicle types to the background and development traffic so they could be easily separated from within the micro-simulation model. This approach is consistent with the GTIA requirements.

Table 4-3 shows an aggregate delay assessment of the network in the existing configuration (no mitigation upgrades), undertaken in accordance with the GTIA. The average vehicle delays for each of the individual intersections within the analysis can be found in the micro-simulation modelling report included in Appendix D.

Table 4-3 Delay Assessment - Existing Configuration

| INTERSECTION | PEAK PERIOD | AGGREGATE INTERSECTION-DELAY (VEHICLE-MINUTES) |  | $\mathrm{ID}=\sum_{i=1}^{n} W D-\sum_{i=1}^{n} B C$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\sum B C$ | $\sum W D$ | $\Delta$ | \% |
| Existing Configuration (No upgrades) | AM Peak | 629,062 | 805,784 | 176,722 | 28.09\% |
|  | PM Peak | 532,573 | 618,853 | 86,280 | 16.2\% |
|  | Combined Peaks | 1,161,635 | 1,424,637 | 263,002 | 22.64\% |

The assessment found that with no mitigation upgrades the development generated traffic would increase the aggregate intersection delay by more than $5 \%$. As such, mitigation works to the network are required.
Due to its proximity to the proposed development site, the Finucane Road / Delancey Street signalised intersection was analysed to determine if mitigation upgrades could be undertaken to improve the performance of the overall surrounding network.
We propose that the form of the Finucane Road / Delancey Street intersection be designed generally as shown in Figure 4-2. Due to traffic volumes and logistically fitting the intersection into the available road reserve, the following intersection configuration in our view is ideal.


Figure 4-2 Proposed Finucane Road / Delancey Street Signalised Intersection Layout

Table 4-4 shows an aggregate delay assessment of the network including the above mitigation upgrades to the Finucane Road / Delancey Street signalised intersection, undertaken in accordance with the GTIA. It should be noted that the reconfiguration of the intersection has resulted in a change to the current signal phasing plan. Details of the updated signal phasing are included in the micro-simulation model report attached in Appendix $\mathbf{D}$. The average vehicle delays for each of the individual intersections within the analysis can be found in the micro-simulation modelling report included in Appendix D.

Table 4-4 Delay Assessment - With Upgrades

| INTERSECTION | PEAK PERIOD | AGGREGATE INTERSECTION-DELAY (VEHICLE-MINUTES) |  | $\mathrm{ID}=\sum_{i=1}^{n} W D-\sum_{i=1}^{n} B C$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\sum B C$ | $\sum W D$ | $\Delta$ | \% |
| Mitigation (With upgrades) | AM Peak | 629,062 | 615,128 | -13,934 | -2.22\% |
|  | PM Peak | 532,573 | 433,418 | -99,155 | -18.62\% |
|  | Combined Peaks | 1,161,635 | 1,048,546 | -113,089 | -9.74\% |

As demonstrated in Table 4-4, the assessment found that the development generated traffic would increase the aggregate intersection delay by less than $5 \%$ if mitigation upgrades are undertaken to the Finucane Road / Delancey Street signalised intersection, as illustrated in Figure 4-2. The results demonstrate that the performance of the network would theoretically improve with the proposed mitigation upgrades, with a decrease in the average delay experienced through the network.

On the basis of the above, and with the implementation of the proposed upgrade works at the intersection of Finucane Road / Delancey Street, in our view that project will result in a "no net worsening" of delay to the
state-controlled road network and on this basis will satisfy the requirements of the SDAP Codes and the GTIA analysis process and guidelines.

The implementation of the proposed upgrade has been contemplated in some detail given the existing corridor widths available and the land ownership constraints. It is noted that the verge on the southern side of the Finucane Road frontage adjacent to the intersection is relatively narrow and while this land appears to be relatively unconstrained it is understood to be owned by the State.

In advancing the conceptual design of the proposed intersection upgrades we note that the project team has developed a solution that appears to be able to be accommodated within the existing road corridor or within land that forms part of the proposal.

The Concept Design for the proposed upgrade works at the subject intersection is shown in the plans prepared by Mortons Urban Solutions which have been informed by the detailed traffic modelling work undertaken and documented above. The concept design of the intersection is included in Drawing No. 37801-XWP-005 Amend. A and included in Appendix F of this report.

It is proposed that these works will be implemented as part of the ultimate project delivery.

### 4.8 ACCESS ARRANGEMENTS - IMPACT ASSESSMENT

### 4.8.1 SIDRA ANALYSIS ASSUMPTIONS

The following scenario provides an assessment of the proposed Finucane Road signalised access intersection as well as the existing priority-controlled access intersection via Delancey Street.

The following parameters have been applied to the SIDRA model:

- A Saturation Flow of 1,950 through car units per hour;
- A Peak Flow Period of 30 minutes, with a conservative Peak Flow Factor of 95\%;
- Heavy vehicle volumes based on the traffic survey count data;
- Intersection geometry based on measurements of aerial imagery supplemented with on-site measurements; and
- Gap acceptance parameters based on default SIDRA values (for the right turn out of Arthur Street at the Delancey Street site access intersection, the gap acceptance parameters outlined in AUSTROADS GTRD Part 4A Table 3.5 for a right turn from minor road across a two-lane / two-way road have been adopted).


### 4.8.2 EXISTING SITE ACCESS ON DELANCEY STREET

SIDRA Intersection software has been used to assess the performance of the Finucane Road signalised access intersection. Figure 4-3 shows the proposed intersection configuration as modelled in the SIDRA analysis.


Figure 4-3 Delancey Street / Site Access / Arthur Street Intersection Layout

Table 4-5 presents the results of the Delancey Street access intersection SIDRA analysis for 2024 and 2034 with development scenarios, with detailed movement summary SIDRA outputs included in Appendix E.

Table 4-5 Delancey Street / Site Access / Arthur Street Intersection SIDRA Outputs

|  | APPROACH |  | AM PEAK |  |  |  | PM PEAK |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SCENARIO |  |  | DoS | Avg Delay (s) | LoS | 95\% <br> Back of Queue (m) | DoS | Avg Delay (s) | LoS | 95\% <br> Back of Queue (m) |
| 2024 Design <br> (Background <br> Development) | Delancey Street (S) | Left | 0.045 | 5.6 | LOS A | 0 | 0.034 | 5.6 | LOS A | 0 |
|  |  | Through | 0.182 | 0 | LOS A | 0 | 0.174 | 0 | LOS A | 0 |
|  |  | Right | 0.008 | 7.7 | LOS A | 0.2 | 0.01 | 6.9 | LOS A | 0.3 |
|  |  | U-turn | 0.008 | 11.7 | LOS B | 0.2 | 0.01 | 9.8 | LOS A | 0.3 |
|  |  | Approach | 0.182 | 1.2 | NA | 0.2 | 0.174 | 1.1 | NA | 0.3 |
|  | Arthur Street (E) | Left | 0.024 | 8.6 | LOS A | 0.5 | 0.014 | 7.5 | LOS A | 0.3 |
|  |  | Right | 0.024 | 18 | LOS C | 0.5 | 0.014 | 14.6 | LOS B | 0.3 |
|  |  | Approach | 0.024 | 11.4 | LOS B | 0.5 | 0.014 | 9.3 | LOS A | 0.3 |
|  | Delancey Street <br> (N) | Left | 0.301 | 5.6 | LOS A | 0 | 0.225 | 5.6 | LOS A | 0 |
|  |  | Through | 0.301 | 0.1 | LOS A | 0 | 0.225 | 0.1 | LOS A | 0 |
|  |  | Right | 0.111 | 7.6 | LOS A | 3.1 | 0.078 | 7.3 | LOS A | 2.1 |
|  |  | U-turn | 0.111 | 9.3 | LOS A | 3.1 | 0.078 | 9.1 | LOS A | 2.1 |
|  |  | Approach | 0.301 | 1.2 | NA | 3.1 | 0.225 | 1.2 | NA | 2.1 |
|  | Site Access (W) | Left | 0.143 | 7.3 | LOS A | 3.7 | 0.199 | 7.4 | LOS A | 5.5 |
|  |  | Approach | 0.143 | 7.3 | LOS A | 3.7 | 0.034 | 5.6 | LOS A | 0 |
| 2034 Design <br> (Background <br> Development) | Delancey Street <br> (S) | Left | 0.045 | 5.6 | LOS A | 0 | 0.034 | 5.6 | LOS A | 0 |
|  |  | Through | 0.244 | 0.1 | LOS A | 0 | 0.194 | 0 | LOS A | 0 |
|  |  | Right | 0.011 | 8.2 | LOS A | 0.3 | 0.011 | 7.1 | LOS A | 0.3 |
|  |  | U-turn | 0.011 | 12.7 | LOS B | 0.3 | 0.011 | 10.2 | LOS B | 0.3 |
|  |  | Approach | 0.244 | 1 | NA | 0.3 | 0.194 | 1 | NA | 0.3 |
|  | Arthur Street (E) | Left | 0.037 | 9.2 | LOS A | 0.8 | 0.017 | 7.7 | LOS A | 0.4 |
|  |  | Right | 0.037 | 23.6 | LOS C | 0.8 | 0.017 | 16.2 | LOS C | 0.4 |
|  |  | Approach | 0.037 | 14 | LOS B | 0.8 | 0.017 | 9.6 | LOS A | 0.4 |
|  | Delancey Street <br> (N) | Left | 0.335 | 5.6 | LOS A | 0 | 0.245 | 5.6 | LOS A | 0 |
|  |  | Through | 0.335 | 0.1 | LOS A | 0 | 0.245 | 0.1 | LOS A | 0 |
|  |  | Right | 0.129 | 8.5 | LOS A | 3.5 | 0.082 | 7.6 | LOS A | 2.2 |
|  |  | U-turn | 0.129 | 10.7 | LOS B | 3.5 | 0.082 | 9.5 | LOS A | 2.2 |
|  |  | Approach | 0.335 | 1.3 | NA | 3.5 | 0.245 | 1.1 | NA | 2.2 |
|  | Site Access (W) | Left | 0.166 | 8.2 | LOS A | 4.2 | 0.208 | 7.6 | LOS A | 5.7 |
|  |  | Approach | 0.045 | 5.6 | LOS A | 0 | 0.034 | 5.6 | LOS A | 0 |

As illustrated in Table 4-5, the Delancey Street access will operate below the practical capacity for a prioritycontrolled intersection (DoS<0.8, Delay<42 sec) at both the year of opening (2024) and a 10-year design horizon (2034) in both peak periods.

### 4.8.3 PROPOSED SITE ACCESS ON FINUCANE ROAD

SIDRA Intersection software has been used to assess the performance of the Finucane Road signalised access intersection. Figure 4-4 shows the proposed intersection configuration as modelled in the SIDRA analysis.


Figure 4-4 Proposed Finucane Road Signalised Access Intersection
The signal phasing plan adopted in both peak periods can be seen in Figure 4-5. A cycle time of 90 seconds has been adopted for this analysis.


Figure 4-5 Finucane Road Signalised Access Intersection Signal Phasing
Table 4-6 presents the results of the Finucane Road access intersection SIDRA analysis with detailed movement and phasing SIDRA Outputs attached in Appendix E.

Table 4-6 Finucane Road Signalised Access Intersection SIDRA Outputs

|  | APPROACH |  | AM PEAK |  |  |  | PM PEAK |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SCENARIO |  |  | DoS | Avg Delay (s) | LoS | 95\% Back of Queue (m) | DoS | Avg Delay (s) | LoS | 95\% <br> Back of Queue (m) |
| 2024 Design <br> (Background + Development) | Finucane Road <br> (E) | Through | 0.595 | 6.9 | LOS A | 126 | 0.601 | 9.4 | LOS A | 133.3 |
|  |  | Right | 0.604 | 47.1 | LOS D | 45.4 | 0.633 | 49.4 | LOS D | 40.9 |
|  |  | Approach | 0.604 | 10.3 | LOS B | 126 | 0.633 | 12.6 | LOS B | 133.3 |
|  | Site Access (N) | Left | 0.212 | 27.3 | LOS C | 30 | 0.249 | 25.5 | LOS C | 37.4 |
|  |  | Right | 0.517 | 44.5 | LOS D | 43.7 | 0.612 | 41.1 | LOS D | 68.6 |
|  |  | Approach | 0.517 | 36.2 | LOS D | 43.7 | 0.612 | 34.4 | LOS C | 68.6 |
|  | Finucane Road <br> (W) | Left | 0.178 | 9.5 | LOS A | 22.4 | 0.143 | 8.8 | LOS A | 16.5 |
|  |  | Through | 0.620 | 16.7 | LOS B | 136.5 | 0.623 | 18.7 | LOS B | 132.6 |
|  |  | Approach | 0.62 | 15.5 | LOS B | 136.5 | 0.623 | 17.2 | LOS B | 132.6 |
| 2034 Design <br> (Background + Development) | Finucane Road (E) | Through | 0.637 | 7.3 | LOS A | 142.1 | 0.641 | 8.8 | LOS A | 147.3 |
|  |  | Right | 0.659 | 48.9 | LOS D | 46.7 | 0.633 | 49.4 | LOS D | 40.9 |
|  |  | Approach | 0.659 | 10.6 | LOS B | 142.1 | 0.641 | 11.7 | LOS B | 147.3 |
|  | Site Access (N) | Left | 0.219 | 28.1 | LOS C | 30.5 | 0.264 | 27.1 | LOS C | 38.8 |
|  |  | Right | 0.670 | 46.4 | LOS D | 59.2 | 0.684 | 44.1 | LOS D | 72.1 |
|  |  | Approach | 0.67 | 38.7 | LOS D | 59.2 | 0.684 | 36.8 | LOS D | 72.1 |
|  | Finucane Road <br> (W) | Left | 0.175 | 9.2 | LOS A | 21.4 | 0.143 | 8.8 | LOS A | 16.5 |
|  |  | Through | 0.713 | 17.1 | LOS B | 170.8 | 0.695 | 18.2 | LOS B | 159.6 |
|  |  | Approach | 0.713 | 15.9 | LOS B | 170.8 | 0.695 | 17 | LOS B | 159.6 |

As illustrated in Table 4-6, the Finucane Road access will operate within the reasonable operational limits for a signalised intersection (notionally $\operatorname{DoS}<0.9$ ) at both the year of opening (2024) and a 10-year design horizon (2034) in both peak periods. Queues on the eastern Finucane Road approach will remain within turn lanes and clear of the adjacent Delancey Street signalised intersection. Queues on the western Finucane Road approach will remain within turn lanes and clear of adjacent intersections.

The operational analysis shows that the proposed signalised intersection would operate at an acceptable level for the ten-year design horizon and importantly all traffic would be able to clear during each relevant phase.

We note that this analysis has been based on the intersection being analysed as an isolated intersection and not part of a network. The micro-simulation model report includes the proposed Finucane Road access intersection, demonstrating that a network-based analysis results in even better operational outcomes that that demonstrated in Table 4-6.

The Concept Design for the site access intersection is shown in the plans prepared by Mortons Urban Solutions which have been informed by the detailed traffic modelling work undertaken and described above. The concept design of the intersection is included in Drawing No. 37801-XWP-005 Amend. A and included in Appendix F of this report.

## 5. SUMMARY

Lambert \& Rehbein (SEQ) Pty Ltd has been commissioned by The Hub Precinct Pty Ltd undertake a Traffic Impact Assessment for a proposed mixed use commercial development located at 58-68 Delancey Street, Ormiston QLD 4160, which is formally described as 0/SP308738, 0-2/SP308739; 0/SP308740; 4/SP308740; and $10-16 /$ SP314782. The development site currently contains existing and approved medical and education buildings, a car park, and a portion of vacant land, with a total site area of approximately 5.2ha.
The proposed designation is for an Integrated Health \& Education Precinct, consisting of a private hospital, medical consulting suites, research and education facility, residential aged care, and ancillary retail." This report has considered the sites full development potential which also includes childcare, independent living and a community hub which will be assessed at a future date via the DA process. It is understood that the development will be completed over three (3) stages. The proposed development proposes to gain access to the external road network via a new signalised intersection on Finucane Road and an existing access on Delancey Street. The proposed site layout, prepared by Destravis Group, is attached in Appendix A.

The development application is being pursued through the Ministerial Designation process and this traffic assessment forms part of the application material.

The development proposes to gain access directly to the State-controlled road network via a new signalised intersection on Finucane Road to the west of the existing Delancey Street intersection. The site will also gain access to the Delancey Street albeit that the existing all-movements access will be reconfigured to remove the right turn egress from the subject land.

Given the intent to provide a new signalised intersection on Delancey Street, the traffic assessment has included undertaking a detailed assessment of the site intersections for a 10 year design horizon beyond the potential year of opening of 2024. This analysis indicated that the proposal for the new signalised intersection can be incorporated into the state-controlled road network in a manner that will achieve an acceptable level of operational efficiency and can be delivered in a manner consistent with the applicable guidelines. Conceptual functional layout plans have been developed for the site access intersection and are shown in Drawing No. 37801-XWP-005 Amend. A and included in Appendix F of this report.

On the basis of the development including a new intersection on the state-controlled road network we have also undertaken a detailed traffic modelling assessment based on a detailed microsimulation modelling approach. This analysis determined that the development, along with the new signalised intersection would have a relatively significant impact on the net delays through the network. As a part of the modelling process assessment of suitable road network options were undertaken and an upgraded layout for the Delancey Street signalised intersection was developed to mitigate the development impacts. The changes proposed can be delivered within the road network, within any land take contained with land that forms part of the application, and deliver a significant net benefit to the network-based delays.

Conceptual functional layout plans for the upgrades at the Finucane Road / Delancey Street intersection and are shown in Drawing No. 37801-XWP-005 Amend. A and included in Appendix F of this report.
Based on the detailed traffic analysis and modelling undertaken we are of the view that the proposal can be supported from a traffic perspective.

## APPENDIX A - SITE PLANS



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|  | ${ }_{\text {ex }}$ |

## APPENDIX B- RAW TRAFFIC SURVEY DATA



| Approach |  |  | McDonald Rd |  |  | Finucane Rd |  |  | McDonald Rd |  |  | Finucane Rd |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  | $\begin{aligned} & \text { 皆 } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { 厄iँ } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { n } \\ & \text { 总 } \end{aligned}$ |  |  | $\begin{aligned} & \text { 吡 } \\ & \text { 品 } \end{aligned}$ |  | $\begin{array}{\|c} \overline{\mathrm{b}} \\ \hline \end{array}$ |  |  | $\begin{gathered} \text { Ði } \\ \hline \end{gathered}$ |  |
| 6：00 | to | 7：00 | 50 | 1 | 51 | 979 | 21 | 1，000 | 87 | 6 | 93 | 554 | 32 | 586 | 1，730 |
| 6：15 | to | 7：15 | 59 | 0 | 59 | 1，056 | 23 | 1，079 | 90 | 5 | 95 | 624 | 35 | 659 | 1，892 |
| 6：30 | to | 7：30 | 60 | 0 | 60 | 1，159 | 26 | 1，185 | 110 | 4 | 114 | 723 | 41 | 764 | 2，123 |
| 6：45 | to | 7：45 | 61 | 0 | 61 | 1，173 | 31 | 1，204 | 120 | 3 | 123 | 808 | 39 | 847 | 2，235 |
| 7：00 | to | 8：00 | 69 | 0 | 69 | 1，206 | 31 | 1，237 | 153 | 3 | 156 | 953 | 49 | 1，002 | 2，464 |
| 7：15 | to | 8：15 | 85 | 0 | 85 | 1，258 | 36 | 1，294 | 205 | 6 | 211 | 1，101 | 50 | 1，151 | 2，741 |
| 7：30 | to | 8：30 | 114 | 1 | 115 | 1，335 | 38 | 1，373 | 254 | 7 | 261 | 1，162 | 50 | 1，212 | 2，961 |
| 7：45 | to | 8：45 | 140 | 2 | 142 | 1，396 | 40 | 1，436 | 291 | 6 | 297 | 1，171 | 52 | 1，223 | 3，098 |
| 8：00 | to | 9：00 | 142 | 2 | 144 | 1，451 | 48 | 1，499 | 280 | 6 | 286 | 1，118 | 44 | 1，162 | 3，091 |
| AM Totals |  |  | 261 | 3 | 264 | 3，636 | 100 | 3，736 | 520 | 15 | 535 | 2，625 | 125 | 2，750 | 7，285 |
| 14：30 | to | 15：30 | 129 | 3 | 132 | 1，136 | 28 | 1，164 | 172 | 3 | 175 | 1，229 | 36 | 1，265 | 2，736 |
| 14：45 | to | 15：45 | 135 | 2 | 137 | 1，175 | 31 | 1，206 | 177 | 5 | 182 | 1，284 | 30 | 1，314 | 2，839 |
| 15：00 | to | 16：00 | 119 | 1 | 120 | 1，217 | 35 | 1，252 | 185 | 8 | 193 | 1，282 | 39 | 1，321 | 2，886 |
| 15：15 | to | 16：15 | 130 | 1 | 131 | 1，188 | 34 | 1，222 | 183 | 7 | 190 | 1，300 | 35 | 1，335 | 2，878 |
| 15：30 | to | 16：30 | 122 | 2 | 124 | 1，231 | 32 | 1，263 | 181 | 6 | 187 | 1，301 | 33 | 1，334 | 2，908 |
| 15：45 | to | 16：45 | 116 | 2 | 118 | 1，241 | 34 | 1，275 | 168 | 3 | 171 | 1，300 | 30 | 1，330 | 2，894 |
| 16：00 | to | 17：00 | 125 | 2 | 127 | 1，269 | 24 | 1，293 | 163 | 0 | 163 | 1，377 | 18 | 1，395 | 2，978 |
| 16：15 | to | 17：15 | 120 | 2 | 122 | 1，291 | 21 | 1，312 | 153 | 0 | 153 | 1，363 | 15 | 1，378 | 2，965 |
| 16：30 | to | 17：30 | 117 | 1 | 118 | 1，222 | 20 | 1，242 | 156 | 0 | 156 | 1，372 | 14 | 1，386 | 2，902 |
| 16：45 | to | 17：45 | 120 | 0 | 120 | 1，159 | 15 | 1，174 | 171 | 0 | 171 | 1，335 | 14 | 1，349 | 2，814 |
| 17：00 | to | 18：00 | 114 | 0 | 114 | 1，021 | 16 | 1，037 | 156 | 0 | 156 | 1，278 | 14 | 1，292 | 2，599 |
| 17：15 | to | 18：15 | 114 | 0 | 114 | 926 | 13 | 939 | 149 | 0 | 149 | 1，194 | 13 | 1，207 | 2，409 |
| 17：30 | to | 18：30 | 101 | 0 | 101 | 793 | 17 | 810 | 141 | 0 | 141 | 1，058 | 8 | 1，066 | 2，118 |
| PM Totals |  |  | 469 | 6 | 475 | 4，382 | 97 | 4，479 | 650 | 9 | 659 | 4，960 | 91 | 5，051 | 10，664 |


| Job No． | ：AUQLD3388 |
| :--- | :--- |
| Client | ：Lambert \＆Rehbein（SEQ）Pty Ltd |
| Suburb | ：Cleveland |
| Location | ： 2 Finucane Rd （ |：2．Finucane Rd／Dawson Rd

Day／Date Tue， 29 Mar 2022WeatherDescription ：Classified Intersection Count：Peak Hour Summary
：Classified Intersection Count
Peak Hour Summary


| Approach |  |  |  | Finucane Rd |  |  | Dawson Rd |  |  | Finucane Rd |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  | $\begin{aligned} & \text { n } \\ & \text { 壹 } \end{aligned}$ |  | 厄i厄 | $\begin{aligned} & \text { 喜 } \\ & \substack{\text { n }} \end{aligned}$ | $\stackrel{\check{0}}{\stackrel{y}{z}}$ | $\overline{\mathrm{g}}$ | $\begin{aligned} & \text { n } \\ & \text { 吉 } \end{aligned}$ |  | $\overline{\mathrm{E}}$ |  |
| AM | 7：45 | to | 8：45 | 1，501 | 41 | 1，542 | 97 | 4 | 101 | 1，431 | 51 | 1，482 | 3，125 |
| PM | 16：00 | to | 17：00 | 1，372 | 30 | 1，402 | 53 | 1 | 54 | 1，450 | 12 | 1，462 | 2，918 |


| Approach | Finucane Rd |  |  | Dawson Rd |  |  | Finucane Rd |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | $\begin{aligned} & \text { n } \\ & \hline \underline{\text { an }} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{y}{0} \\ & \stackrel{0}{x} \end{aligned}$ | $\begin{gathered} \text { 厄iّ } \\ \hline \end{gathered}$ |  |  | $\stackrel{\text { 「 }}{\stackrel{5}{6}}$ |  | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{y}{0} \\ & \text { anx } \end{aligned}$ | $\begin{gathered} \text { 厄゙厄 } \\ \hline \end{gathered}$ |  |
| 6：00 to 7：00 | 1，009 | 26 | 1，035 | 51 | 2 | 53 | 624 | 33 | 657 | 1，745 |
| 6：15 to 7：15 | 1，148 | 25 | 1，173 | 60 | 2 | 62 | 674 | 40 | 714 | 1，949 |
| 6：30 to 7：30 | 1，209 | 33 | 1，242 | 60 | 3 | 63 | 771 | 34 | 805 | 2，110 |
| 6：45 to 7：45 | 1，229 | 36 | 1，265 | 66 | 2 | 68 | 869 | 41 | 910 | 2，243 |
| 7：00 to 8：00 | 1，299 | 35 | 1，334 | 78 | 1 | 79 | 1，041 | 50 | 1，091 | 2，504 |
| 7：15to <br> $8: 15$ | 1，340 | 43 | 1，383 | 90 | 1 | 91 | 1，269 | 46 | 1，315 | 2，789 |
| 7：30 to 8：30 | 1，412 | 39 | 1，451 | 102 | 2 | 104 | 1，380 | 57 | 1，437 | 2，992 |
| 7：45to <br> $8: 45$ | 1，501 | ${ }^{41}$ | 1，542 | 97 | 4 | 101 | 1，431 | 51 | 1，482 | 3，125 |
| 8：00 to 9：00 | 1，483 | 52 | 1，535 | 93 | 5 | 98 | 1，364 | 44 | 1，408 | 3，041 |
| AM Totals | 3，791 | 113 | 3，904 | 222 | 8 | 230 | 3，029 | 127 | 3，156 | 7，290 |
| 14：30to <br> $15: 30$ | 1，266 | 32 | 1，298 | 53 | 2 | 55 | 1，430 | 39 | 1，469 | 2，822 |
| 14：45 to $15: 45$ | 1，323 | 42 | 1，365 | 55 | 4 | 59 | 1，414 | 40 | 1，454 | 2，878 |
| 15：00 to 16：00 | 1，280 | 45 | 1，325 | 54 | 3 | 57 | 1，439 | 37 | 1，476 | 2，858 |
| 15：15 to $16: 15$ | 1，358 | 44 | 1，402 | 51 | 3 | 54 | 1，411 | 36 | 1，447 | 2，903 |
| 15：30 to $16: 30$ | 1，339 | 45 | 1，384 | 59 | 3 | 62 | 1，356 | 29 | 1，385 | 2，831 |
| 15：45 to 16：45 | 1，356 | 35 | 1，391 | 51 | 1 | 52 | 1，418 | 19 | 1，437 | 2，880 |
| 16：00 to 17：00 | 1，372 | 30 | 1，402 | 53 | 1 | 54 | 1，450 | 12 | 1，462 | 2，918 |
| 16：15 $\quad$ to 17715 | 1，285 | 25 | 1，310 | 57 | 2 | 59 | 1，457 | 11 | 1，468 | 2，837 |
| 16：30 to 17730 | 1，277 | 19 | 1，296 | 55 | 3 | 58 | 1，462 | 11 | 1，473 | 2，827 |
| 16：45 $\quad$ to 17745 | 1，158 | 18 | 1，176 | 63 | 3 | 66 | 1，383 | 14 | 1，397 | 2，639 |
| 17：00 to 18：00 | 1，071 | 14 | 1，085 | 64 | 4 | 68 | 1，343 | 13 | 1，356 | 2，509 |
| 17：15 $\quad$ to $18: 15$ | 962 | 18 | 980 | 55 | 3 | 58 | 1，228 | 10 | 1，238 | 2，276 |
| 17：30 to 18：30 | 845 | 16 | 861 | 58 | 3 | 61 | 1，103 | 10 | 1，113 | 2，035 |
| PM Totals | 4，727 | 112 | 4，839 | 225 | 11 | 236 | 5，351 | 89 | 5，440 | 10，515 |




| Approach |  |  | Delancey St |  |  | Shore St $\mathbf{W}$ |  |  | Delancey St |  |  | Finucane Rd |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  | $\begin{aligned} & \text { n } \\ & \text { 喜 } \\ & \hline \end{aligned}$ |  | $\begin{gathered} \text { Ð. } \\ \stackrel{\rightharpoonup}{\circ} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { 皆 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{y}{0} \\ & \stackrel{y}{2} \\ & \text { ax } \end{aligned}$ | $\begin{array}{\|} \stackrel{\text { ®. }}{\circ} \\ \hline \end{array}$ | $\begin{aligned} & \text { n } \\ & \stackrel{y}{2} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { u } \\ & \stackrel{0}{2} \\ & \text { axi } \end{aligned}$ | $\begin{gathered} \text { Ð. } \\ \stackrel{\rightharpoonup}{\circ} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { n} \\ & \substack{\text { non } \\ \hline} \\ & \hline \end{aligned}$ |  | $\begin{array}{\|c} \text { Ð. } \\ \stackrel{\rightharpoonup}{\circ} \\ \hline \end{array}$ |  |
| 6:00 | to | 7:00 | 434 | 8 | 442 | 554 | 12 | 566 | 152 | 4 | 156 | 643 | 30 | 673 | 1,837 |
| 6:15 | to | 7:15 | 479 | 9 | 488 | 666 | 16 | 682 | 191 | 5 | 196 | 719 | 43 | 762 | 2,128 |
| 6:30 | to | 7:30 | 498 | 11 | 509 | 695 | 24 | 719 | 240 | 5 | 245 | 820 | 35 | 855 | 2,328 |
| 6:45 | to | 7:45 | 556 | 15 | 571 | 707 | 22 | 729 | 260 | 5 | 265 | 932 | 40 | 972 | 2,537 |
| 7:00 | to | 8:00 | 606 | 13 | 619 | 733 | 26 | 759 | 339 | 5 | 344 | 1,097 | 52 | 1,149 | 2,871 |
| 7:15 | to | 8:15 | 673 | 15 | 688 | 746 | 27 | 773 | 410 | 8 | 418 | 1,309 | 43 | 1,352 | 3,231 |
| 7:30 | to | 8:30 | 711 | 12 | 723 | 805 | 25 | 830 | 483 | 10 | 493 | 1,454 | 56 | 1,510 | 3,556 |
| 7:45 | to | 8:45 | 727 | 10 | 737 | 890 | 32 | 922 | 511 | 11 | 522 | 1,492 | 53 | 1,545 | 3,726 |
| 8:00 | to | 9:00 | 706 | 14 | 720 | 879 | 36 | 915 | 492 | 13 | 505 | 1,422 | 47 | 1,469 | 3,609 |
| AM Totals |  |  | 1,746 | 35 | 1,781 | 2,166 | 74 | 2,240 | 983 | 22 | 1,005 | 3,162 | 129 | 3,291 | 8,317 |
| 14:30 | to | 15:30 | 583 | 8 | 591 | 837 | 27 | 864 | 366 | 6 | 372 | 1,437 | 39 | 1,476 | 3,303 |
| 14:45 | to | 15:45 | 606 | 13 | 619 | 805 | 30 | 835 | 447 | 10 | 457 | 1,426 | 40 | 1,466 | 3,377 |
| 15:00 | to | 16:00 | 604 | 11 | 615 | 786 | 28 | 814 | 476 | 12 | 488 | 1,444 | 41 | 1,485 | 3,402 |
| 15:15 | to | 16:15 | 670 | 10 | 680 | 785 | 27 | 812 | 439 | 12 | 451 | 1,420 | 37 | 1,457 | 3,400 |
| 15:30 | to | 16:30 | 642 | 12 | 654 | 794 | 24 | 818 | 428 | 12 | 440 | 1,396 | 33 | 1,429 | 3,341 |
| 15:45 | to | 16:45 | 678 | 11 | 689 | 830 | 18 | 848 | 384 | 6 | 390 | 1,442 | 22 | 1,464 | 3,391 |
| 16:00 | to | 17:00 | 652 | 10 | 662 | 859 | 18 | 877 | 417 | 3 | 420 | 1,443 | 13 | 1,456 | 3,415 |
| 16:15 | to | 17:15 | 579 | 9 | 588 | 849 | 14 | 863 | 437 | 1 | 438 | 1,470 | 12 | 1,482 | 3,371 |
| 16:30 | to | 17:30 | 570 | 7 | 577 | 857 | 13 | 870 | 429 | 3 | 432 | 1,448 | 12 | 1,460 | 3,339 |
| 16:45 | to | 17:45 | 490 | 3 | 493 | 780 | 14 | 794 | 389 | 4 | 393 | 1,399 | 16 | 1,415 | 3,095 |
| 17:00 | to | 18:00 | 453 | 1 | 454 | 712 | 13 | 725 | 335 | 5 | 340 | 1,354 | 16 | 1,370 | 2,889 |
| 17:15 | to | 18:15 | 409 | 1 | 410 | 641 | 15 | 656 | 296 | 6 | 302 | 1,239 | 14 | 1,253 | 2,621 |
| 17:30 | to | 18:30 | 355 | 3 | 358 | 568 | 12 | 580 | 257 | 3 | 260 | 1,140 | 11 | 1,151 | 2,349 |
| PM Totals |  |  | 2,150 | 30 | 2,180 | 3,056 | 76 | 3,132 | 1,480 | 24 | 1,504 | 5,421 | 95 | 5,516 | 12,332 |



|  | Approach |  |  | Wellington St |  |  | Shore St W |  |  | Wellington St |  |  | Shore St W |  |  |  |
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| AM | 8：00 | to | 9：00 | 589 | 33 | 622 | 938 | 32 | 970 | 823 | 19 | 842 | 1，119 | 30 | 1，149 | 3，583 |
| PM | 16：15 | to | 17：15 | 619 | 8 | 627 | 1，011 | 21 | 1，032 | 603 | 9 | 612 | 1，068 | 9 | 1，077 | 3，348 |


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| 6：00 | to | 7：00 | 283 | 28 | 311 | 514 | 15 | 529 | 366 | 4 | 370 | 423 | 26 | 449 | 1，659 |
| 6：15 | to | 7：15 | 325 | 19 | 344 | 567 | 14 | 581 | 420 | 4 | 424 | 467 | 33 | 500 | 1，849 |
| 6：30 | to | 7：30 | 349 | 25 | 374 | 628 | 19 | 647 | 495 | 3 | 498 | 550 | 36 | 586 | 2，105 |
| 6：45 | to | 7：45 | 395 | 26 | 421 | 674 | 20 | 694 | 561 | 9 | 570 | 641 | 33 | 674 | 2，359 |
| 7：00 | to | 8：00 | 424 | 26 | 450 | 717 | 20 | 737 | 614 | 13 | 627 | 763 | 41 | 804 | 2，618 |
| 7：15 | to | 8：15 | 458 | 27 | 485 | 763 | 26 | 789 | 697 | 16 | 713 | 896 | 41 | 937 | 2，924 |
| 7：30 | to | 8：30 | 507 | 27 | 534 | 836 | 23 | 859 | 738 | 20 | 758 | 1，026 | 34 | 1，060 | 3，211 |
| 7：45 | to | 8：45 | 561 | 30 | 591 | 892 | 25 | 917 | 811 | 19 | 830 | 1，118 | 38 | 1，156 | 3，494 |
| 8：00 | to | 9：00 | 589 | 33 | 622 | 938 | 32 | 970 | 823 | 19 | 842 | 1，119 | 30 | 1，149 | 3，583 |
|  | Tot |  | 1，296 | 87 | 1，383 | 2，169 | 67 | 2，236 | 1，803 | 36 | 1，839 | 2，305 | 97 | 2，402 | 7，860 |
| 14：30 | to | 15：30 | 550 | 21 | 571 | 914 | 24 | 938 | 610 | 17 | 627 | 975 | 31 | 1，006 | 3，142 |
| 14：45 | to | 15：45 | 561 | 16 | 577 | 895 | 21 | 916 | 631 | 17 | 648 | 1，090 | 25 | 1，115 | 3，256 |
| 15：00 | to | 16：00 | 555 | 15 | 570 | 864 | 19 | 883 | 671 | 19 | 690 | 1，105 | 30 | 1，135 | 3，278 |
| 15：15 | to | 16：15 | 586 | 12 | 598 | 829 | 16 | 845 | 698 | 20 | 718 | 1，106 | 25 | 1，131 | 3，292 |
| 15：30 | to | 16：30 | 605 | 12 | 617 | 856 | 14 | 870 | 674 | 17 | 691 | 1，112 | 26 | 1，138 | 3，316 |
| 15：45 | to | 16：45 | 614 | 13 | 627 | 955 | 20 | 975 | 655 | 14 | 669 | 1，013 | 23 | 1，036 | 3，307 |
| 16：00 | to | 17：00 | 636 | 10 | 646 | 979 | 20 | 999 | 629 | 12 | 641 | 1，018 | 12 | 1，030 | 3，316 |
| 16：15 | to | 17：15 | 619 | 8 | 627 | 1，011 | 21 | 1，032 | 603 | 9 | 612 | 1，068 | 9 | 1，077 | 3，348 |
| 16：30 | to | 17：30 | 598 | 6 | 604 | 984 | 21 | 1，005 | 618 | 8 | 626 | 1，087 | 9 | 1，096 | 3，331 |
| 16：45 | to | 17：45 | 601 | 4 | 605 | 918 | 20 | 938 | 610 | 5 | 615 | 1，078 | 10 | 1，088 | 3，246 |
| 17：00 | to | 18：00 | 554 | 7 | 561 | 840 | 16 | 856 | 608 | 4 | 612 | 1，055 | 12 | 1，067 | 3，096 |
| 17：15 | to | 18：15 | 515 | 8 | 523 | 755 | 16 | 771 | 617 | 4 | 621 | 973 | 12 | 985 | 2，900 |
| 17：30 | to | 18：30 | 479 | 5 | 484 | 680 | 14 | 694 | 551 | 3 | 554 | 905 | 9 | 914 | 2，646 |
| PM Totals |  |  | 2，232 | 44 | 2，276 | 3，434 | 73 | 3，507 | 2，453 | 45 | 2，498 | 4，079 | 75 | 4，154 | 12，435 |


| Job No． | ：AUQLD3388 |
| :--- | :--- |
| Client | ：Lambert \＆Rehbein（SEQ）Pty Ltd |
| Suburb | $:$ Cleveland |
| Location | $: 5$. Wellington St／Russell St |
|  |  |
| Day／Date | ：Tue，29 Mar 2022 |
| Weather | ：Fine |
| Description | $:$ Classified Intersection Count |
|  | $:$ Peak Hour Summary |




| Approach |  |  | Wellington St |  |  | Russell St |  |  | Wellington St |  |  | Russell St |  |  |  |
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| 6：00 | to | 7：00 | 442 | 25 | 467 | 208 | 3 | 211 | 380 | 17 | 397 | 148 | 4 | 152 | 1，227 |
| 6：15 | to | 7：15 | 482 | 17 | 499 | 239 | 5 | 244 | 374 | 15 | 389 | 191 | 4 | 195 | 1，327 |
| 6：30 | to | 7：30 | 530 | 18 | 548 | 246 | 5 | 251 | 445 | 9 | 454 | 227 | 4 | 231 | 1，484 |
| 6：45 | to | 7：45 | 556 | 26 | 582 | 252 | 3 | 255 | 500 | 7 | 507 | 252 | 3 | 255 | 1，599 |
| 7：00 | to | 8：00 | 586 | 24 | 610 | 308 | 5 | 313 | 563 | 12 | 575 | 274 | 2 | 276 | 1，774 |
| 7：15 | to | 8：15 | 641 | 22 | 663 | 358 | 4 | 362 | 630 | 18 | 648 | 320 | 3 | 323 | 1，996 |
| 7：30 | to | 8：30 | 665 | 26 | 691 | 422 | 7 | 429 | 631 | 21 | 652 | 386 | 6 | 392 | 2，164 |
| 7：45 | to | 8：45 | 713 | 23 | 736 | 497 | 9 | 506 | 622 | 27 | 649 | 447 | 10 | 457 | 2，348 |
| 8：00 | to | 9：00 | 715 | 24 | 739 | 491 | 9 | 500 | 578 | 28 | 606 | 440 | 11 | 451 | 2，296 |
| AM Totals |  |  | 1，743 | 73 | 1，816 | 1，007 | 17 | 1，024 | 1，521 | 57 | 1，578 | 862 | 17 | 879 | 5，297 |
| 14：30 | to | 15：30 | 653 | 22 | 675 | 335 | 4 | 339 | 519 | 28 | 547 | 399 | 11 | 410 | 1，971 |
| 14：45 | to | 15：45 | 692 | 18 | 710 | 355 | 6 | 361 | 534 | 26 | 560 | 403 | 10 | 413 | 2，044 |
| 15：00 | to | 16：00 | 683 | 17 | 700 | 344 | 5 | 349 | 559 | 24 | 583 | 414 | 11 | 425 | 2，057 |
| 15：15 | to | 16：15 | 753 | 14 | 767 | 335 | 4 | 339 | 581 | 20 | 601 | 437 | 12 | 449 | 2，156 |
| 15：30 | to | 16：30 | 757 | 14 | 771 | 345 | 6 | 351 | 587 | 18 | 605 | 464 | 8 | 472 | 2，199 |
| 15：45 | to | 16：45 | 746 | 14 | 760 | 340 | 6 | 346 | 594 | 13 | 607 | 479 | 7 | 486 | 2，199 |
| 16：00 | to | 17：00 | 742 | 9 | 751 | 361 | 7 | 368 | 566 | 12 | 578 | 519 | 4 | 523 | 2，220 |
| 16：15 | to | 17：15 | 692 | 7 | 699 | 329 | 7 | 336 | 592 | 8 | 600 | 542 | 2 | 544 | 2，179 |
| 16：30 | to | 17：30 | 675 | 5 | 680 | 296 | 5 | 301 | 589 | 8 | 597 | 540 | 2 | 542 | 2，120 |
| 16：45 | to | 17：45 | 626 | 4 | 630 | 280 | 2 | 282 | 565 | 8 | 573 | 511 | 2 | 513 | 1，998 |
| 17：00 | to | 18：00 | 593 | 6 | 599 | 232 | 1 | 233 | 550 | 8 | 558 | 478 | 2 | 480 | 1，870 |
| 17：15 | to | 18：15 | 583 | 6 | 589 | 209 | 1 | 210 | 515 | 7 | 522 | 439 | 2 | 441 | 1，762 |
| 17：30 | to | 18：30 | 530 | 6 | 536 | 192 | 1 | 193 | 491 | 5 | 496 | 386 | 3 | 389 | 1，614 |
| PM Totals |  |  | 2，615 | 47 | 2，662 | 1，168 | 16 | 1，184 | 2，186 | 59 | 2，245 | 1，789 | 24 | 1，813 | 7，904 |




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| 6：00 | to | 7：00 | 310 | 15 | 325 | 0 | 0 | 0 | 358 | 2 | 360 | 45 | 1 | 46 | 731 |
| 6：15 | to | 7：15 | 346 | 18 | 364 | 3 | 0 | 3 | 418 | 1 | 419 | 62 | 1 | 63 | 849 |
| 6：30 | to | 7：30 | 392 | 19 | 411 | 6 | 0 | 6 | 473 | 3 | 476 | 72 | 1 | 73 | 966 |
| 6：45 | to | 7：45 | 439 | 23 | 462 | 6 | 0 | 6 | 530 | 7 | 537 | 73 | 1 | 74 | 1，079 |
| 7：00 | to | 8：00 | 462 | 20 | 482 | 6 | 0 | 6 | 589 | 12 | 601 | 102 | 2 | 104 | 1，193 |
| 7：15 | to | 8：15 | 508 | 17 | 525 | 5 | 0 | 5 | 624 | 13 | 637 | 123 | 1 | 124 | 1，291 |
| 7：30 | to | 8：30 | 553 | 16 | 569 | 2 | 0 | 2 | 680 | 12 | 692 | 167 | 6 | 173 | 1，436 |
| 7：45 | to | 8：45 | 563 | 17 | 580 | 4 | 0 | 4 | 684 | 11 | 695 | 212 | 7 | 219 | 1，498 |
| 8：00 | to | 9：00 | 557 | 18 | 575 | 4 | 0 | 4 | 637 | 12 | 649 | 214 | 7 | 221 | 1，449 |
|  | Tota |  | 1，329 | 53 | 1，382 | 10 | 0 | 10 | 1，584 | 26 | 1，610 | 361 | 10 | 371 | 3，373 |
| 14：30 | to | 15：30 | 648 | 11 | 659 | 8 | 1 | 9 | 552 | 14 | 566 | 136 | 3 | 139 | 1，373 |
| 14：45 | to | 15：45 | 655 | 9 | 664 | 9 | 1 | 10 | 547 | 17 | 564 | 165 | 3 | 168 | 1，406 |
| 15：00 | to | 16：00 | 667 | 9 | 676 | 19 | 0 | 19 | 575 | 19 | 594 | 164 | 2 | 166 | 1，455 |
| 15：15 | to | 16：15 | 714 | 7 | 721 | 34 | 0 | 34 | 538 | 15 | 553 | 159 | 2 | 161 | 1，469 |
| 15：30 | to | 16：30 | 728 | 7 | 735 | 39 | 0 | 39 | 524 | 15 | 539 | 162 | 2 | 164 | 1，477 |
| 15：45 | to | 16：45 | 749 | 7 | 756 | 39 | 0 | 39 | 522 | 12 | 534 | 140 | 2 | 142 | 1，471 |
| 16：00 | to | 17：00 | 743 | 6 | 749 | 32 | 0 | 32 | 504 | 9 | 513 | 125 | 2 | 127 | 1，421 |
| 16：15 | to | 17：15 | 769 | 6 | 775 | 14 | 0 | 14 | 524 | 8 | 532 | 142 | 2 | 144 | 1，465 |
| 16：30 | to | 17：30 | 761 | 6 | 767 | 10 | 0 | 10 | 537 | 3 | 540 | 129 | 1 | 130 | 1，447 |
| 16：45 | to | 17：45 | 768 | 5 | 773 | 9 | 0 | 9 | 503 | 2 | 505 | 112 | 1 | 113 | 1，400 |
| 17：00 | to | 18：00 | 739 | 7 | 746 | 15 | 0 | 15 | 515 | 2 | 517 | 117 | 1 | 118 | 1，396 |
| 17：15 | to | 18：15 | 665 | 7 | 672 | 25 | 0 | 25 | 470 | 0 | 470 | 86 | 1 | 87 | 1，254 |
| 17：30 | to | 18：30 | 629 | 7 | 636 | 25 | 0 | 25 | 423 | 0 | 423 | 80 | 1 | 81 | 1，165 |
| PM Totals |  |  | 2，766 | 31 | 2，797 | 82 | 1 | 83 | 2，036 | 32 | 2，068 | 507 | 7 | 514 | 5，462 |




| Approach | Delancey St |  |  | Freeth St W |  |  | Delancey St |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | $\begin{aligned} & \text { n } \\ & \text { 喜 } \\ & \hline \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & \text { n } \\ & \stackrel{5}{\mathrm{y}} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { u } \\ & \stackrel{0}{2} \\ & \text { axi } \end{aligned}$ | $\begin{gathered} \text { 厄゙ँ } \\ \hline \end{gathered}$ |  |  |
| 6：00 to 7：00 | 101 | 0 | 101 | 58 | 3 | 61 | 159 | 3 | 162 |  | 324 |
| 6：15 to 7：15 | 134 | 2 | 136 | 80 | 3 | 83 | 205 | 2 | 207 |  | 426 |
| 6：30 to 7：30 | 149 | 3 | 152 | 90 | 2 | 92 | 250 | 2 | 252 |  | 496 |
| 6：45 to 7：45 | 184 | 4 | 188 | 103 | 2 | 105 | 282 | 3 | 285 |  | 578 |
| 7：00 to 8：00 | 231 | 8 | 239 | 126 | 2 | 128 | 344 | 3 | 347 |  | 714 |
| 7：15 ${ }^{\text {to }} 8: 15$ | 318 | 9 | 327 | 139 | 3 | 142 | 401 | 4 | 405 |  | 874 |
| 7：30 to 8：30 | 404 | 14 | 418 | 160 | 3 | 163 | 496 | 11 | 507 |  | 1，088 |
| 7：45 $\quad$ to $8: 45$ | 438 | 17 | 455 | 182 | 3 | 185 | 596 | 12 | 608 |  | 1，248 |
| 8：00 $\quad$ to 9：00 | 426 | 15 | 441 | 173 | 4 | 177 | 571 | 12 | 583 |  | 1，201 |
| AM Totals | 758 | ${ }^{23}$ | 781 | 357 | 9 | 366 | 1，074 | 18 | 1，092 |  | 2，239 |
| 14：30 to 15：30 | 412 | 9 | 421 | 164 | 5 | 169 | 292 | 4 | 296 |  | 886 |
| 14：45 to 15：45 | 440 | 11 | 451 | 167 | 6 | 173 | 386 | 8 | 394 |  | 1，018 |
| 15：00 to 16：00 | 387 | 10 | 397 | 150 | 8 | 158 | 441 | 8 | 449 |  | 1，004 |
| 15：15 to 16：15 | 369 | 10 | 379 | 143 | 6 | 149 | 396 | 10 | 406 |  | 934 |
| 15：30 to 16：30 | 356 | 9 | 365 | 132 | 3 | 135 | 388 | 11 | 399 |  | 899 |
| 15：45 to 16：45 | 363 | 6 | 369 | 150 | 2 | 152 | 345 | 5 | 350 |  | 871 |
| 16：00 to 17：00 | 378 | 4 | 382 | 153 | 0 | 153 | 352 | 4 | 356 |  | 891 |
| 16：15 to 17：15 | 377 | 3 | 380 | 155 | 0 | 155 | 389 | 1 | 390 |  | 925 |
| 16：30 to 17：30 | 379 | 4 | 383 | 174 | 2 | 176 | 375 | 3 | 378 |  | 937 |
| 16：45 to 17：45 | 346 | 5 | 351 | 170 | 2 | 172 | 316 | 4 | 320 |  | 843 |
| 17：00 to 18：00 | 320 | 6 | 326 | 176 | 3 | 179 | 273 | 4 | 277 |  | 782 |
| 17：15 to 18：15 | 286 | 6 | 292 | 165 | 3 | 168 | 239 | 5 | 244 |  | 704 |
| 17：30 to 18：30 | 243 | 4 | 247 | 139 | 1 | 140 | 202 | 2 | 204 |  | 591 |
| PM Totals | 1，390 | 26 | 1，416 | 609 | 11 | 620 | 1，257 | 20 | 1，277 |  | 3，313 |

## APPENDIX C- TRAFFIC MOVEMENT DIAGRAMS








## APPENDIX D- MICRO SIMLUATION MODELLING REPORT

## a <br> danner

## Private Hospital Finuc ane ROAD - AcCESS ANALYSIS

Mic ro-simulation modelling

Analysis of the traffic impacts of a proposed private hospital with access onto Finucane Road, Cleveland

Charles Reeler
Version 1
8/07/2022

Prepared by Adanner Pty Ltd for [insert client name]

Report version control

| Version | Date | Author | Change Description |
| :---: | :---: | :---: | :---: |
| 1 | $8 / 07 / 2022$ | Charles Reeler | DRAFT |
| 2 | $8 / 07 / 2022$ | Charles Reeler | FINAL |
|  |  |  |  |

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## TABLE OF CONTENTS

1 Background ..... 4
2 Methodology ..... 5
2.1 Study Area ..... 5
2.2 Proposed Land Use and Trip Generation ..... 6
2.3 Simulation Model Network ..... 9
2.4 Traffic Signal Data ..... 10
2.5 Model Software ..... 11
2.6 Calibration of 2022 Ba se Case Models ..... 11
2.6.1 R-Squared ..... 12
2.6.2 Tum Volume Calibration ..... 13
3 Modelling Results ..... 17
3.1 Performance Criteria ..... 17
3.2 Modelled Scenarios. ..... 17
3.2.1 Scena rio 1 - Existing Situation ..... 18
3.2.2 Scenario 2 - Existing Network with Development Traffic ..... 19
3.2.3 Scenario 3 - Upgrade 1 . ..... 21
3.2.4 Scenario 4 - Upgrade 2 ..... 23
3.2.5 Scenario 5 - Upgrade 3. ..... 25
3.3 Intersection Performance ..... 25
3.4 Network Performance ..... 26
4 Conclusions ..... 28

## 1 BACKGROUND

A private hospital with mixed-use development has been proposed to be developed on the corner of Finucane Road and Delancey Street in Cleveland. There is an existing access on Delancey Street servicing the current development however with further development of this site this existing access will be inadequate for the predicted traffic demands.
A second access to the development site is therefore proposed on Finucane Road to meet the increased traffic demands to and from the site.

The purpose of this document is to provide the results of an assessment of the traffic impacts of proposed development at the new Finucane Road access, the impact of the development on the surrounding road network and to identify mitigating measures to address the increased traffic demands.

This report documents the findings of the micro-simulation modelling carried out for this investigation.

## 2 METHODOLOGY

### 2.1 Study Area

Figure 1 shows the site of the private hospital and proposed mixed development and the surrounding road network that has been included in the simulation modelling.
The study area extends from McDonald Road in the west to Wellington Street in the east and from Russel Street in the south to Freeth Street in the north. Seven intersections are included in the study are as shown in the figure below.


Figure 1 Study Area
The intersections included in the models are:

1. Finucane Road / McDonald Road
2. Finucane Road / Dawson Road
3. Finucane Road / Delancey Street
4. Finucane Road / Wellington Street
5. Wellington Street / Russel Street
6. Wellington Street / Freeth Street
7. Delancey Street / Freeth Street

The development site is located in the north west corner of the intersection of Finucane Road and Delancey Street. There is an existing access to the current site off Delancey Street opposite the Arthur Street intersection. The new second access is proposed off Finucane Road at the western end of the development site as shown below (site dimensions and access location - not to scale).


Figure 2 Site Location and Accesses

### 2.2 Proposed Land Use and Tip Generation

Previous studies investigating the proposed development and accesses have been carried out by Lambert \& Rehbein (L\&R). These studies include detailed trip generation rates for the development as well as assignment to and from the development site for the weekday AM and PM peak periods. These assumptions are documented in the L\&R document titled: "Technical Note - Proposed Hospital ad M ixed Use Development, Cnr Finucane Road \& Delancey Street, Qld 4160, Access Intersection Analysis", dated 10/11/2021.

For the purposes of this analysis, the same trip generation and assignment assumptions have been assumed (albeit with slight changes as described in the following sections). In summary the proposed development mix is presented in the following table (extract from the L\&R document):

| USE | YIELD |  |
| :--- | :---: | :---: |
| PRIVATE HOSPITAL | 148 BEDS + 14 THEATRES | $22,411 \mathrm{~m}^{2}$ GFA |
| DAY SURGERY | 18 Day Beds |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | - | $1,200 \mathrm{~m}^{2}$ GFA |
| CHILD CARE | 150 PLACES | $6,213 \mathrm{~m}^{2}$ GFA |
| SPECIAL RETAIL | - | $4,407 \mathrm{~m}^{2}$ GFA |
| RESEARCH INSTITUTE | - | $25,000 \mathrm{~m}^{2}$ GFA |
| ASSISTED LIVING UNIT \& FACILITIES | 200 UNITS + FACILITIES | $11,163 \mathrm{~m}^{2}$ GFA |
| AGED CARE | 134 BEDS + Ancilary Area | $2,000 \mathrm{~m}^{2}$ GFA |
| COMMUNITY HUB | - | $77,008 \mathrm{~m}^{2}$ GFA |
| TOTAL |  |  |

## Table 1 Proposed Development Yields

Based on these yields the trip generation for the development was estimated using the trip generation rates and directionality as shown in the following table.

| LAND USE | GENERATION RATE |  | DIRECTIONALITY (\% IN / \% OUT) |  | SOURCE |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak | PM Peak | AM Peak | PM Peak |  |
| PRIVATE HOSPITAL | $\begin{aligned} & -22.07 \text { trips }+1.04 \\ & \text { trips } \times \text { beds } \end{aligned}$ | $\begin{gathered} -22.07 \text { trips }+1.04 \\ \text { trips } \times \text { beds } \end{gathered}$ | 50\% in / 50\% out | $50 \%$ in / 50\% out | RMS (formally RTA) |
| DAY SURGERY |  |  |  |  |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | ${\underset{\text { GFA }}{ } 9.81 \text { trips / } 100 \mathrm{~m}^{2}}^{\text {and }}$ | $\begin{gathered} 5.80 \text { trips } / 100 \mathrm{~m}^{2} \\ \text { GFA } \end{gathered}$ | $50 \%$ in / 50\% out | $50 \%$ in / $50 \%$ out | DTMR Open Source Data |
| CHILD CARE | 0.8 trips / child | 0.7 trips / child | $50 \%$ in / $50 \%$ out | $50 \%$ in / 50\% out | RMS (formally RTA) |
| SPECIAL RETAIL | 2.8 trips / $100 \mathrm{~m}^{2}$ GFA | 5.6 trips / $100 \mathrm{~m}^{2}$ GFA | $50 \%$ in / $50 \%$ out | $50 \%$ in / $50 \%$ out | RMS (formally RTA) |
| RESEARCH INSTITUTE | 2 trips / $100 \mathrm{~m}^{2}$ GFA | 2 trips / $100 \mathrm{~m}^{2}$ GFA | 90\% in / 10\% out | 10\% in / $90 \%$ out | RMS (formally RTA) |
| ASSISTED LIVING UNIT \& FACILITIES | 0.2 trips per dwelling | 0.2 trips per dwelling | $80 \%$ in / $20 \%$ out | 20\% in / 80\% out | RMS (formally RTA) |
| AGED CARE | 0.2 trips per dwelling | 0.2 trips per dwelling | $80 \%$ in / $20 \%$ out | 20\% in / 80\% out | RMS (formally RTA) |

## Table 2 Trip Generation and Directionality Rates

With these laned uses and trip generation assumptions, the trip generation of the development was determined as follows:

| LAND USE | YIELD | AM(IN) | AM (OUT) | PM (IN) | PM (OUT) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PRIVATE HOSPITAL | $\begin{gathered} 148 \text { BEDS + } 14 \\ \text { THEATRES } \end{gathered}$ | 75 | 75 | 75 | 75 |
| DAY SURGERY | 18 Day Beds |  |  |  |  |
| MEDICAL SPECIALISTS IN CONSULTING SUITES BLDG | 4,614 m ${ }^{2}$ GFA | 226 | 226 | 134 | 134 |
| CHILD CARE | 150 PLACES | 60 | 60 | 53 | 53 |
| SPECIAL RETAIL | 6,213 m ${ }^{2}$ GFA | 87 | 87 | 174 | 174 |
| RESEARCH INSTITUTE | $4,407 \mathrm{~m}^{2}$ GFA | 79 | 9 | 9 | 79 |
| ASSISTED LIVING UNIT \& FACILITIES | 200 UNITS + FACILITIES | 32 | 8 | 8 | 32 |
| AGED CARE | 134 BEDS + Ancillary Area | 21 | 5 | 5 | 21 |
| COMMUNITY HUB | 2,000 m ${ }^{2}$ GFA | - | - | - | - |
| Total Trips per Peak (10\% Cross-Utilisation) |  | 524 | 424 | 412 | 512 |

Table 3 Development Traffic Generation
These trips were then assigned with the basic assumptions that the existing access on Delancey Road would attract $20 \%$ of the trips and the new Finucane Road access would attract the remaining $80 \%$ of the trips.
For the purposes of this micro-simulation analysis these assumptions were slightly modified.
The current access on Delancey Street allows all movements. With the proposed development the movements at this access will change to left-in, left-out and right-in only. No right-turns out of the site onto Delancey Street will be permitted. As a result, the assumption is that vehicles leaving the site and travelling south to Wellington Street and Russell Street will use the main access on Finucane Road.
It was also assumed that vehicles to and from the west on Finucane Road would all use the "M ain" access on Finucane Road rather than travel past this access to the access on Delancey Street. Similarly, it was assumed that vehicles to and from Delancey Street (to the north) and Wellington Street (to the north) would all use the Delancey Street access rather than travel past this access to the Finucane Road access. These assumptions are illustrated in the following figures showing the routes to and from the two access points from the various trip generation zones.


Figure $3 \quad$ Trips to and from Finucane Road access


Figure $4 \quad$ Trips to and from Delancey Street access
With these assumptions the original 80:20 split between the Finucane Road and Delancey Street accesses changed to 77:23.

| Directional Split <br> between accesses | Original split |  | Reassigned split |  |
| :--- | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM |
| Finucane | $80 \%$ | $80 \%$ | $77 \%$ | $77 \%$ |
| Delancey | $20 \%$ | $20 \%$ | $23 \%$ | $23 \%$ |

Table 4 Directional Split of Trips to and from the Development
The trip generation (OD matrices) for this reassignment is shown in more detail in Annexure A.

### 2.3 Simulation Model Network

As mentioned previously, the study area comprises

- Finucane Road from M cDonald Road in the west to Wellington Street in the east
- Wellington Street from Russel Street in the south to Freeth Street in the north
- Delancey Street / Russel Street from Wellington Street in the south to Freeth Street in the north

There are 7 intersections in the network with 11 'external' trip generation zones. Additional zones were added to the network to act as sinks or generators to balance the trips arriving at and departing from the seven intersections where traffic count data is known.

In addition, an $8^{\text {th }}$ intersection was added at the location of the proposed new access to the development on Finucane Road. The development site was also allocated two separate zones, one for the Finucane Road access and one for the Delancey Street access. The full simulation network showing the trip generation zones and the new access is presented in the following figure. Zones 15 and 18 are the zones allocated to the development.


Figure 5 Simulation network and trip generation zones

### 2.4 Traffic Signal Data

Traffic signal data was provided for the following intersections:

- Finucane Road / McDonald Road
- Finucane Road / Delancey Street
- Wellington Street / Russell Street

The data provided comprised the signal phase sequences and actual timing data (length of time for each phase in M ay 2022). While the signal phasing data specifies the cycle lengths during the peak periods ( 160 sec AM peak and 130 sec PM Peak), the actual phase times data varies so that the actual cycle times varied and were not always equal to the stated cycle times.

For the purposes of the modelling, it was therefore assumed that the signals are isolated and operate under actuated control in the Base case models. The limits of the variability of the signal phases were then set to the minimums and maximums as recorded in the data provided.

### 2.5 Model Software

The simulation software used for this analysis is AIM SUN Next 20 (Version 20). (Note that using a different version of the software may result in slight changes to the results).

### 2.6 Calibration of 2022 Base Case Models

For this analysis, the Base M odel is defined as the 2022 network as the calibration is based on the turn count data collected in M arch 2022.
The initial demand matrices were derived by assignment of trips between zones using a proportional distribution based on the volumes of attractions and generations to and from each zone. The models were then run to generate modelled turn flows at each intersection which were then compared to the count data. Based on these results, some manual adjustments were made to specific OD pairs so that an acceptable calibration could be achieved. The final manual adjustments included adding trips to and from the internal 'sink' zones. This iterative process was carried out until suitable calibration was achieved.

While route choices in the models are limited, there are certain route choices that required some minor adjustments to the default attributes in the software. Attribute overrides (additional delays) were applied at two locations, namely:

- In the AM Peak at the Wellington / Finucane roundabout (four movements)
- In the AM Peak at the Wellington / Russell intersection (two movements)
- In the PM peak at the Wellington / Finucane and the Wellington / Freeth roundabouts (four movements)
- In the AM Peak at the Wellington / Russell intersection (two movements)

In addition to these changes a number of OD routes were defined to prevent unrealistic route choices:

- Between Finucane east and Finucane west (both directions)
- From Finucane east to Wellington south
- From Finucane east to Russel Street

All models were run for 2 hours (one hour warm-up and the second hour used for all the result reporting). Five seed values were used to replicate the natural variability in daily traffic patterns and all results are based on the average of the five simulation runs. The best calibration was achieved using a proportional distribution whilst allowing on-route path updates using 5-minute calculation intervals.

The criteria for calibration of simulation models are typically based on the R-squared statistic and GEH values (comparison between actual intersection count data and the modelled turn volumes). The calibration criteria with the values from the models is shown in Table 2.

| Calibration Criteria | Actual achieved |  |
| :--- | :---: | :---: |
|  | AM | PM |
| R-squared >0.9 | 0.987 | 0.979 |
| GEH <5 in at least 85\% of observations | $93 \%$ | $94 \%$ |

Table $5 \quad$ Calibration Criteria

### 2.6.1 R-Squared

The R-squared statistic is presented in the following graphs showing the goodness of fit between the intersection counts and the modelled turn volumes for each peak period.


Figure 6
R-Squared Values for 2022 Base models
These graphs show that the models replicate the count data very well with the R-squared statistic well within the recommended limits.

### 2.6.2 Tum Volume Calibration

The tables below shows the GEH values for the turn volumes at the intersections for each peak hour.

|  |  |  |  | COUNT Data |  | M odelled Volumes |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak PM Peak |  | AM Peak |  | PM Peak |  |
| Intersection | Approach | Description | Turn | Total | Total | Total | GEH | Total | GEH |
| 1 Finucane / <br> McDonald | South | McDonald | L | 3 | 14 | 4 | 0.3 | 15 | 0.1 |
|  |  |  | T | 34 | 25 | 35 | 0.1 | 21 | 0.6 |
|  |  |  | R | 105 | 88 | 97 | 0.5 | 87 | 0.1 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | East | Finucane | L | 98 | 117 | 105 | 0.5 | 124 | 0.5 |
|  |  |  | T | 1,276 | 1,101 | 1,309 | 0.7 | 1,123 | 0.5 |
|  |  |  | R | 62 | 75 | 65 | 0.3 | 80 | 0.4 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | North | McDonald | L | 218 | 87 | 207 | 0.5 | 88 | 0.0 |
|  |  |  | T | 32 | 32 | 31 | 0.1 | 31 | 0.1 |
|  |  |  | R | 47 | 44 | 53 | 0.6 | 42 | 0.2 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | West | Finucane | L | 31 | 63 | 32 | 0.1 | 56 | 0.6 |
|  |  |  | T | 1,181 | 1,319 | 1,144 | 0.8 | 1,358 | 0.7 |
|  |  |  | R | 9 | 13 | 11 | 0.5 | 14 | 0.2 |
|  |  |  | U | 2 | 0 | 0 | 1.4 | 0 |  |
| 2 Finucane / <br> Dawson | South |  | L | 0 | 0 | 0 |  | 0 |  |
|  |  |  | T | 0 | 0 | 0 |  | 0 |  |
|  |  |  | R | 0 | 0 | 0 |  | 0 |  |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | East | Finucane | L | 0 | 0 | 0 |  | 0 |  |
|  |  |  | T | 1,458 | 1,292 | 1,459 | 0.0 | 1,313 | 0.4 |
|  |  |  | R | 84 | 110 | 107 | 1.7 | 129 | 1.2 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | North | Dawson | L | 89 | 42 | 80 | 0.7 | 37 | 0.6 |
|  |  |  | T | 0 | 0 | 0 |  | 0 |  |
|  |  |  | R | 12 | 12 | 25 | 2.2 | 17 | 1.0 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | West | Finucane | L | 16 | 21 | 0 | 4.0 | 0 | 4.6 |
|  |  |  | T | 1,466 | 1,441 | 1,451 | 0.3 | 1,538 | 1.8 |
|  |  |  | R | 0 | 0 | 0 |  | 0 |  |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
| 3 Finucane / Delancey | South | Delancey | L | 538 | 506 | 514 | 0.8 | 441 | 2.1 |
|  |  |  | T | 175 | 123 | 104 | 4.2 | 105 | 1.2 |
|  |  |  | R | 24 | 33 | 11 | 2.1 | 19 | 1.9 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | East | Finucane | L | 20 | 25 | 23 | 0.5 | 0 | 4.9 |
|  |  |  | T | 770 | 744 | 751 | 0.5 | 778 | 0.9 |
|  |  |  | R | 113 | 66 | 130 | 1.1 | 56 | 0.9 |
|  |  |  | U | 19 | 42 | 0 | 4.4 | 28 | 1.7 |
|  | North | Delancey | L | 129 | 113 | 103 | 1.7 | 81 | 2.3 |
|  |  |  | T | 133 | 149 | 91 | 2.8 | 162 | 0.7 |
|  |  |  | R | 260 | 157 | 260 | 0.0 | 223 | 3.4 |
|  |  |  | U | 0 | 1 | 0 |  | 0 | 1.0 |
|  | West | Finucane | L | 204 | 202 | 241 | 1.8 | 214 | 0.6 |
|  |  |  | T | 1,060 | 882 | 976 | 1.9 | 1,008 | 2.9 |
|  |  |  | R | 281 | 372 | 300 | 0.8 | 336 | 1.4 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
| 4 Finucane / Wellington | South | Wellington | L | 163 | 153 | 78 | 5.5 | 190 | 2.0 |
|  |  |  | T | 342 | 399 | 208 | 5.7 | 230 | 6.7 |
|  |  |  | R | 83 | 93 | 77 | 0.5 | 127 | 2.3 |
|  |  |  | U | 3 | 1 | 0 | 1.7 | 0 | 1.0 |
|  | East | Finucane | L | 52 | 111 | 66 | 1.3 | 87 | 1.7 |
|  |  |  | T | 658 | 625 | 596 | 1.7 | 654 | 0.8 |
|  |  |  | R | 201 | 250 | 221 | 1.0 | 252 | 0.1 |
|  |  |  | U | 6 | 13 | 0 | 2.4 | 0 | 3.6 |
|  | North | Wellington | L | 245 | 209 | 296 | 2.2 | 192 | 0.8 |
|  |  |  | T | 451 | 334 | 405 | 1.6 | 248 | 3.6 |
|  |  |  | R | 127 | 92 | 182 | 3.1 | 71 | 1.6 |
|  |  |  | U | 7 | 6 | 0 | 2.6 | 0 | 2.4 |
|  | West | Finucane | L | 85 | 102 | 84 | 0.0 | 138 | 2.3 |
|  |  |  | T | 680 | 598 | 687 | 0.2 | 624 | 0.7 |
|  |  |  | R | 331 | 275 | 314 | 0.7 | 348 | 2.9 |
|  |  |  | U | 60 | 55 | 5 | 6.8 | 19 | 4.2 |


|  |  |  |  | COUNT Data |  | M odelled Volumes |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM Peak PM Peak |  | AM Peak |  | PM Peak |  |
| Intersection | Approach | Description | Turn | Total | Total | Total | GEH | Total | GEH |
| 5 Wellington/ Russell | South | Wellington | L | 244 | 252 | 296 | 2.2 | 297 | 1.9 |
|  |  |  | T | 414 | 443 | 314 | 3.7 | 395 | 1.7 |
|  |  |  | R | 77 | 55 | 79 | 0.1 | 60 | 0.5 |
|  |  |  | U | 1 | 1 | 0 | 1.0 | 0 | 1.0 |
|  | East | Russell | L | 42 | 43 | 44 | 0.2 | 46 | 0.3 |
|  |  |  | T | 360 | 247 | 297 | 2.4 | 137 | 5.6 |
|  |  |  | R | 104 | 78 | 103 | 0.1 | 205 | 7.5 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | North | Wellington | L | 55 | 64 | 135 | 5.8 | 182 | 7.5 |
|  |  |  | T | 571 | 493 | 569 | 0.0 | 466 | 0.9 |
|  |  |  | R | 23 | 19 | 2 | 4.3 | 39 | 2.7 |
|  |  |  | U | 0 | 2 | 0 |  | 0 | 1.4 |
|  | West | Russell | L | 19 | 31 | 1 | 3.9 | 51 | 2.2 |
|  |  |  | T | 161 | 201 | 97 | 4.0 | 86 | 6.8 |
|  |  |  | R | 277 | 291 | 276 | 0.0 | 314 | 0.9 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
| 6 Wellington / Freeth | South | Wellington | L | 109 | 115 | 78 | 2.3 | 77 | 2.7 |
|  |  |  | T | 402 | 549 | 418 | 0.6 | 526 | 0.7 |
|  |  |  | R | 15 | 18 | 15 | 0.0 | 16 | 0.4 |
|  |  |  | U |  |  |  |  | 0 |  |
|  | East | Freeth | L | 2 | 23 | 3 | 0.6 | 24 | 0.2 |
|  |  |  | T | 1 | 2 | 0 | 0.7 | 2 | 0.2 |
|  |  |  | R | 1 | 7 | 0 | 1.0 | 6 | 0.3 |
|  |  |  | U |  |  |  |  | 0 |  |
|  | North | Wellington | L | 1 | 3 | 1 | 0.3 | 4 | 0.4 |
|  |  |  | T | 631 | 461 | 646 | 0.4 | 441 | 0.7 |
|  |  |  | R | 59 | 39 | 58 | 0.1 | 77 | 3.5 |
|  |  |  | U |  |  |  |  | 0 |  |
|  | West | Freeth | L | 63 | 59 | 72 | 0.8 | 105 | 3.6 |
|  |  |  | T | 3 | 2 | 2 | 0.4 | 4 | 0.7 |
|  |  |  | R | 151 | 63 | 235 | 4.3 | 45 | 1.8 |
|  |  |  | U |  |  |  |  | 0 |  |
| 7 Delancey/ Freeth | South | Delancey | L | 0 | 0 | 0 |  | 0 |  |
|  |  |  | T | 398 | 312 | 331 | 2.5 | 231 | 3.5 |
|  |  |  | R | 57 | 69 | 126 | 5.1 | 135 | 4.6 |
|  |  |  | U | 0 | 1 | 0 |  | 0 | 1.0 |
|  | East | Freeth | L | 100 | 64 | 66 | 2.6 | 89 | 2.0 |
|  |  |  | T | 0 | 0 | 0 |  | 0 |  |
|  |  |  | R | 84 | 89 | 69 | 1.2 | 69 | 1.6 |
|  |  |  | U | 1 | 0 | 0 | 1.0 | 0 |  |
|  | North | Delancey | L | 142 | 61 | 186 | 2.5 | 20 | 4.5 |
|  |  |  | T | 466 | 295 | 387 | 2.7 | 326 | 1.2 |
|  |  |  | R | 0 | 0 | 0 |  | 0 |  |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
| 8 Delancey / Arthur | South | Delancey | L | 41 | 27 | 37 | 0.5 | 29 | 0.2 |
|  |  |  | T | 463 | 503 | 436 | 0.9 | 337 | 5.7 |
|  |  |  | R | 5 | 5 | 3 | 0.8 | 9 | 1.0 |
|  |  |  | U | 1 | 1 | 0 | 1.0 | 0 | 1.0 |
|  | East | Arthur | L | 7 | 8 | 5 | 0.6 | 7 | 0.3 |
|  |  |  | T | 0 | 0 | 0 |  | 0 |  |
|  |  |  | R | 3 | 1 | 5 | 0.8 | 2 | 0.5 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |
|  | North | Delancey | L | 1 | 7 | 3 | 1.0 | 2 | 1.6 |
|  |  |  | T | 631 | 508 | 438 | 5.9 | 404 | 3.4 |
|  |  |  | R | 12 | 15 | 14 | 0.3 | 11 | 0.8 |
|  |  |  | U | 1 | 1 | 0 | 1.0 | 0 | 1.0 |
|  | West | Site Access | L | 14 | 39 | 16 | 0.4 | 26 | 1.6 |
|  |  |  | T | 0 | 0 | 0 |  | 0 |  |
|  |  |  | R | 13 | 29 | 9 | 0.8 | 52 | 2.6 |
|  |  |  | U | 0 | 0 | 0 |  | 0 |  |

## Table 62022 Base model GEH Values for all turn movements

The focus of the calibration exercise was to replicate the turn volumes at the Finucane Road / Delancey Street intersection as this is the intersection likely to be the most affected by the
development traffic. GEH values of less than 5 (green cells) have been achieved for 93\% and 94\% of all turn movements in the AM and PM peak periods respectively. All the turn movements at the Finucane Road / Delancey Street intersection have GEH values of 5 or less. This is well within the recommended guidelines for calibration. M ore detailed calibration data including light and heavy vehicles volumes is included in Annexure $B$.

The 2022 Base models are therefore considered to be fit for purpose to be used to evaluate the impact of the proposed new access to the development on Finucane Road.

## 3 MODEUNG RESULTS

### 3.1 Performance Criteria

The modelling evaluates the operation of the network and intersections during the weekday AM and PM peak periods. The count data indicates that the peak hours at the Finucane / Delancey intersection are as follows:

- AM Peak: 7:45am to 8:45am
- PM Peak: 4:00pm to 5:00 pm

These peak hours were therefore adopted for the models. The models were all run for 2 hours, one hour prior to the peak hour (warm-up period), and one hour representing the peak hour. Demands from zones on Finucane Road (east and west), M cDonald Road, Russel Street and Wellington Street were profiled so that the releases into the network match the count data profiles.

All models were run with five seed values (RTA specified: 28, $560,2859,7771,86524$ ) and the reported results are the average for the five seeds.
The performance of the intersections is based on the modelled delays for all turn movements. The approach and intersection delays are a weighted average of the individual turn delays. The LOS criteria for signalized intersections, roundabouts and sign-controlled intersections are as per the following table (same criteria as used by SIDRA):

| SIDRA LOS <br> Criteria | Signal | Sign controlled | Roundabout |
| :---: | :---: | :---: | :---: |
| A | 10 | 10 | 10 |
| B | 20 | 15 | 20 |
| C | 35 | 25 | 35 |
| D | 55 | 35 | 50 |
| E | 80 | 50 | 70 |
| F | $>80$ | $>50$ | $>70$ |

Table 7 Level of Service Criteria (seconds)

### 3.2 Modelled Scenarios

To quantify the impact of the development traffic and the proposed upgrades to mitigate the impacts, the following scenarios were modelled:

| Scenario | Network | Demands | Signals |
| :--- | :--- | :--- | :--- |
| 1 | Base (existing) | Background <br> traffic | Existing |
| 2 | Base +development <br> access | Background + <br> development | Existing |
| 3 | Base +development <br> access + Upgrade 1 | Background + <br> development | Revised for Upgrade 1 |
| 4 | Base +development <br> access + Upgrade 2 | Background + <br> development | Revised for Upgrade 2 |

Table 8
Modelled Scenarios

### 3.2.1 Scenario 1 - Existing Situation

These models represent the current operating conditions and serve as a base line or reference against which the other models are compared. As mentioned previously, the Base models used the signal phase times (as provided) and operate under actuated control. With these assumptions and signal control, a suitable calibration was achieved.
The Base model network in the vicinity of the development site is shown in the figure below.


Figure $7 \quad$ Base Model Network
The most important intersection in the network is the Finucane Road / Delancey Street intersection and this intersection effectively controls the operation of the traffic through the
simulation network in the vicinity of the development. The signal phase sequence used in the Base models (as per the data provided) is as follows:


Figure 8 Finucane/Delancey Intersection - Base Model Signal Phase Sequence
The signal data provided and used in the models is contained in Annexure E .

### 3.2.2 Scenario 2 - Existing Network with Development Traffic

This scenario comprises the inclusion of the development traffic and the new access on Finucane Road to the development. No other changes are made to the road network or the signal operation at the Finucane Road / Delancey Street intersection. The purpose of this scenario is to illustrate the impact the development traffic would have on the road network without any upgrades.

The development access on Finucane Road has a separate right-turn into the development (signalised and only triggered on demand) and two exiting lanes from the development site, also only triggered on demand.


Figure $9 \quad$ Base Network with Development Accesses
The layout of the Finucane Road access intersection is shown below.


Figure 10 Access to Development site from Finucane Road
The signal phasing at this intersection is designed to minimise delays to the through traffic. The proposed signal phasing at the intersection is as follows:


Figure 11 Signal Phasing - Finucane Road Development Access

### 3.2.3 Scenario 3 - Upgrade 1

The simulation models showed that some delays can occur on the NB approach to the Finucane Road / Delancey Street intersection. Northbound through vehicles on Delancey Street can queue at the stop line of the intersection with queues extending south on Delancey Street to beyond the start of the left-turn slip-lane from Delancey Street to Finucane Road. When this happens, the vehicles turning left cannot get into the left-turn lane and are delayed. To reduce the delays for these vehicles, a potential upgrade would be to extend the left-turn slip-lane so that leftturning vehicles have the ability to get into the left-turn lane without being delayed behind the stopped through traffic. This is shown in the figure below.


Figure 12 Upgrade Option 1 - Lengthened left-turn slip lane from Delancey Street to Finucane Road

In addition to these changes, the lane arrangement on the Delancey Street north approach was also altered by changing the lane configuration from a right-turn lane and a through lane to a right-turn lane and a shared through/right-turn lane.


Figure 13 Finucane Road / Delancey Street - Lane arrangement
As the Finucane Road access intersection is relatively close to the Finucane Road / Delancey Street intersection (approximately 330m), the signals have been co-ordinated to encourage progression and to minimise delays. As a result, the signal phasing at the Finucane Road / Delancey Street intersection is no longer isolated but runs actuated and is co-ordinated with the signal at the development site access. The cycle times used are 160 seconds in the AM peak and 130 seconds in the PM peak (as these are the cycle times that are specified in the signal data received).
With this arrangement, it was found that some benefits could be achieved by some changes to the signal phasing at the Finucane Road / Delancey Street intersection by introducing a rightturn phase from Finucane Road EB to Delancey Street SB (last phase in the sequence below). (Note that this additional phase is already in the options for the signal currently in use however the data provided appears to indicate that this signal phase was not triggered).


Figure 14 Finucane/Delancey Intersection - Upgrade 1 Signal Phasing with Development

### 3.2.4 Scenario 4 - Upgrade 2

In this scenario a further upgrade to the Finucane Road / Delancey Street intersection is proposed comprising the addition of a second right-turn lane from Finucane Road EB to Delancey Street SB. This will require some widening of Delancey Street south of the intersection to accommodate the dual right-turn lanes. This "Upgrade 2" option is shown in the figure below.


Figure $15 \quad$ Upgrade Option 2 - Dual right-turn lane Finucane Road to Delancey Street
With this option the previous signal phases are not appropriate because the opposing rightturns (4 ${ }^{\text {th }}$ phase - EB to SB and WB to NB) cannot occur in the same phase. The signal phase sequence proposed for this option is as follows:


Figure 16 Finucane/Delancey Intersection - Upgrade 2 Signal Phasing with Development and dual right-turn lanes

The additional capacity provided by the second right-turn lane from Finucane Road means that more green time can be allocated to the east-west through movements as well as to the traffic on the Delancey Street north and south approaches to the intersection. This also encourages traffic to use Delancey Street to Wellington Street rather than proceeding east on Finucane Road to Wellington Street via the Wellington Street / Finucane Road roundabout which is the most congested during peak periods.

### 3.2.5 Scenario 5 - Upgrade 3

This scenario is similar to Scenario 4 but with a relatively minor change to the lane arrangement on Finucane Road east approach to the intersection. In this option the left-turn movement is combined with the through movement in the kerbside lane with a through lane and a right-turn lane.

This "Upgrade 3" option is shown in the figure below.


Figure $17 \quad$ Upgrade Option 3 - Dual right-turn lane Finucane Road to Delancey Street
Changing this east approach may help facilitate providing the dual right-turn lanes on the west approach while minimising the construction impacts.

### 3.3 Intersection Performance

The performance of the network is based on the modelled delays at all the intersections in the network. From the model outputs the intersection level of service (LOS) can then be determined for each turn movement, each approach and each intersection. A summary of the intersection performance results using delay as the performance metric to determine the LOS is shown in the table below.

| Intersection LOS | AM |  |  |  |  | PM |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Scenario 1 | Scenario 2 | Scenario 3 | Scenario 4 | Scenario 5 | Scenario 1 | Scenario 2 | Scenario 3 | Scenario 4 | Scenario 5 |
| Intersection | Base Network | Base + development | Base with development + $\text { Upgrade } 1$ | Base with development + Upgrade 2 | $\qquad$ | Base Network | Base + development | Base with development + Upgrade 1 | Base with development + Upgrade 2 | Base with development + Upgrade 2 |
| 1 Finucane / McDonald | C | C | D | C | C | C | C | C | C | C |
| 2 Finucane / Dawson | A | A | A | A | A | A | A | A | A | A |
| 3 Finucane / Delancey | E | E | E | D | D | E | E | D | C | C |
| 4 Finucane / Wellington | C | D | C | C | C | B | C | C | C | C |
| 5 Wellington / Russell | E | E | F | E | E | D | D | F | D | D |
| 6 Wellington / Freeth | A | A | A | A | A | A | A | A | A | A |
| 7 Delancey / Freeth | E | F | F | C | C | A | A | A | A | A |
| 8 Delancey / Arthur | D | B | B | A | A | E | A | A | A | A |
| 9 Finucane / Site Access |  | B | B | , | C |  | C | , | B | B |

Table 9 Intersection Performance - Level of Service
The associated average vehicle delays for the LOS metrics are presented in the following table.

| Intersection delays | AM |  |  |  |  | PM |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Scenario 1 | Scenario 2 | Scenario 3 | Scenario 4 | Scenario 5 | Scenario 1 | Scenario 2 | Scenario 3 | Scenario 4 | Scenario 5 |
| Intersection | Base Network | Base + development | Base with development + Upgrade 1 | $\begin{gathered} \text { Base with } \\ \text { development + } \\ \text { Upgrade 2 } \\ \hline \end{gathered}$ | Base with development + Upgrade 3 | Base Network | Base + development | $\begin{array}{\|c\|} \hline \text { Base with } \\ \text { development + } \\ \text { Upgrade 1 } \end{array}$ | Base with development + Upgrade 2 | $\begin{array}{\|c\|} \hline \text { Base with } \\ \text { development }+ \\ \text { Upgrade 2 } \\ \hline \end{array}$ |
| 1 Finucane / McDonald | 32.8 | 34.6 | 35.5 | 34.2 | 33.7 | 31.8 | 30.7 | 30.9 | 30.6 | 31.0 |
| 2 Finucane / Dawson | 3.5 | 3.6 | 3.1 | 3.1 | 3.2 | 3.8 | 4.0 | 3.2 | 3.3 | 3.4 |
| 3 Finucane / Delancey | 60.2 | 76.1 | 58.0 | 48.6 | 49.5 | 61.9 | 68.3 | 35.7 | 32.0 | 33.4 |
| 4 Finucane / Wellington | 23.4 | 38.0 | 29.1 | 31.9 | 24.7 | 17.7 | 26.4 | 24.4 | 21.2 | 20.6 |
| 5 Wellington / Russell | 60.0 | 75.2 | 80.3 | 77.7 | 77.6 | 45.6 | 50.0 | 54.4 | 50.6 | 50.2 |
| 6 Wellington / Freeth | 4.8 | 7.3 | 3.9 | 3.3 | 3.0 | 3.3 | 2.9 | 3.9 | 2.8 | 3.0 |
| 7 Delancey/ Freeth | 49.3 | 74.5 | 56.8 | 22.4 | 23.0 | 8.5 | 7.5 | 6.9 | 3.7 | 2.2 |
| 8 Delancey / Arthur | 33.8 | 13.9 | 12.9 | 7.3 | 7.6 | 44.3 | 6.5 | 8.5 | 5.9 | 4.2 |
| 9 Finucane / Site Access |  | 16.3 | 11.4 | 13.1 | 22.1 |  | 24.7 | 13.5 | 13.1 | 16.8 |

These results indicate that with the identified intersection upgrades similar intersection performance and delays to the original background vehicles can be achieved even with the development traffic added to the overall traffic demands.
(While no upgrades at the Wellington Road / Russell Street intersection were tested, the model suggest that some relatively minor upgrades to this intersection could result in further network performance benefits).

Annexure C contains more detailed results showing the intersection performance metrics for each scenario.

### 3.4 Network Performance

An overall performance measure for the network can be defined as the sum of all the delays at all the intersections. This is simply the sum of each turn movement multiplied by the associated delay for that turn movement for all intersections in the network. This calculation produces a number that is indicative of the total delay for all intersections in the network.
As before, the Base network can be used as a point of reference to determine the impact the development will have on delays. TM R require mitigation measures to be implemented so that the vehicles in the original Base network, or original background traffic, is not adversely affected by the new development traffic and the associated increases in delays that these vehicles will cause.

To do this comparison, the base case for the background traffic is determined. This is the reference "delay number".

The background traffic turn volumes through all the intersections are multiplied by the "new" delays for each turn movement with the development traffic. Note that because some upgrades or changes to the network have been proposed, the routes taken by the original background traffic may have changed from their original routing to take advantage of the upgrades and improvements. For example, background traffic previously travelling from Finucane Road west to Wellington Street south may have travelled via Finucane Road through Finucane Road / Wellington Street roundabout. With the intersection upgrades at Delancey Street, some of these vehicles may choose to turn right into Delancey Street as this route option may be quicker.

With the simulation models this calculation is easily done by defining different vehicle types for the background traffic and the development traffic. The development traffic vehicles are then simply multiplied by the associated turn delays at all intersection to produce the new "delay number" for the upgraded network.

The table below presents the results of these calculations.

| Background Traffic (Sum of turn volume x delay) |  | Total Delays (sec) |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | AM | PM | Both peaks |  |
| Network Scenario | Total | Total | All traffic |  |
| Scenario 1: Base existing network | 629062 | 532573 | 1161636 |  |
| Scenario 2: Base existing network with development | 805784 | 618853 | 1424637 |  |
| Scenario 3: Development +Upgrade 1 (lengthen slip-lane) | 691710 | 474789 | 1166498 |  |
| Scenario 4: Development +Upgrade 2 (slip lane +dual rights) | 615284 | 433747 | 1049031 |  |
| Scenario 5: Development +Upgrade 3 (slip lane +dual rights +re-alignment) | 615128 | 433418 | 1048546 |  |

Table $11 \quad$ Background Traffic Total Delay (sum of vehs x delay)
These results show that with the development traffic, there could be some additional delays to the background traffic, particularly during the AM peak. With Upgrade 1 the delays are mitigated to some extent with the overall delay for both peaks somewhat less than the delays in the original Base network. However, the delays during the AM peak still exceed the AM peak delays in the Base network.

With Upgrade 2 the total delays to the background vehicles in both peaks are reduced when compared with the delays in the Base network. The percentage increase or decrease in delays is shown in the following table.

| Background traffic \% Increase in delay vs Base | AM | PM | Both peaks |
| :--- | :---: | :---: | :---: |
| Network Scenario | Total | Total | All traffic |
| Scenario 2: Base existing network with development | $28.1 \%$ | $16.2 \%$ | $22.6 \%$ |
| Scenario 3: Development +Upgrade 1 (lengthen slip-lane) | $10.0 \%$ | $-10.9 \%$ | $0.4 \%$ |
| Scenario 4: Development +Upgrade 2 (slip lane +dual rights) | $-2.2 \%$ | $-18.6 \%$ | $-9.7 \%$ |
| Scenario 5: Development +Upgrade 3 (slip lane +dual rights +re-alignment) | $-2.2 \%$ | $-18.6 \%$ | $-9.7 \%$ |

Table 12
Percentage increase in delays to Background Traffic vs Existing Base Network

## 4 CONCLUSIONS

Based on the results of the simulation models, it is concluded that:

- The current network functions relatively well but some intersections, namely the Finucane Road / Delancey Street and the Wellington Road / Russell Street intersections, can be prone to congestion during peak periods.
- The development traffic will impact the performance of the network with the greatest impact likely to occur at the Finucane Road / Delancey Street intersection.
- With the development traffic added to the existing background traffic, delays can be expected to increase. However, these delays can largely be mitigated through some targeted network upgrades in conjunction with traffic signal operation changes.
- The current signal phasing will need to change so that the signals at the access to the development and the signals at the Finucane Road / Delancey Street intersection are vehicle actuated and coordinated with a common cycle time.
- The proposed upgrades are expected to encourage the use of the Delancey Steet connection between Finucane Road and Wellington Road. As a result, this is likely to impact the operation of the Wellington Road / Russell Street intersection which may require further localised upgrades to improve the operation at this location. (No evaluation of any upgrades at this intersection were investigated in this analysis)
- Upgrades 2 and 3 are expected to provide the best result in terms of reduced delays to the existing background traffic in both peak periods due to the significant increased capacity at the Finucane Road / Delancey Street intersection.
- There is little difference between Upgrades 2 and 3 (Scenarios 4 and 5) as the left-turn demand from Finucane Road WB to Delancey Street SB is very low and can easily be combined with the WB through traffic without a significant impact on the intersection performance.


## Annexure A - 2022 Demand Matrices (Weekday AM and PM Peaks)

This Annexure shows the original trip generation to and from the development site and the change in the assumptions regarding the use of the accesses.

Simulation Model Zones


Simulation Model Background Traffic Demands - 2022 AM Peak

| AM Light | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | $\mathbf{1 5}$ | $\mathbf{1 6}$ | $\mathbf{1 7}$ | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0 | $\mathbf{3 0}$ | 0 | 90 | 138 | 6 | 495 | 0 | 58 | 318 | 0 | 0 | 1 | 9 | $\mathbf{1 3}$ | 0 | 0 | $\mathbf{1 1 5 8}$ |
| $\mathbf{2}$ | 47 | 0 | 0 | 20 | 0 | 0 | 110 | 0 | 13 | 71 | 0 | 0 | 0 | 30 | 0 | 0 | 0 | $\mathbf{2 9 1}$ |
| $\mathbf{3}$ | 25 | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 4 | 24 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | $\mathbf{9 4}$ |
| $\mathbf{4}$ | 239 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 229 | 50 | 0 | 1 | 0 | 9 | 0 | 0 | $\mathbf{5 7 0}$ |
| $\mathbf{5}$ | 164 | 0 | 0 | 0 | 0 | 3 | 247 | 70 | 29 | 159 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{6 7 2}$ |
| $\mathbf{6}$ | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{4}$ |
| $\mathbf{7}$ | 369 | 29 | 44 | 101 | 155 | 7 | 0 | 0 | 65 | 0 | 0 | 0 | 2 | 43 | 15 | 0 | 0 | $\mathbf{8 3 0}$ |
| $\mathbf{8}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{9}$ | 206 | 16 | 25 | 56 | 86 | 0 | 0 | 0 | 0 | 40 | 0 | 0 | 1 | 24 | 8 | 0 | 0 | $\mathbf{4 6 2}$ |
| $\mathbf{1 0}$ | 250 | 19 | 30 | 68 | 105 | 5 | 80 | 0 | 75 | 0 | 0 | 0 | 1 | 29 | 10 | 0 | 0 | $\mathbf{6 7 2}$ |
| $\mathbf{1 1}$ | 0 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{5 0}$ |
| $\mathbf{1 2}$ | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{4 0}$ |
| $\mathbf{1 3}$ | 2 | 0 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{9}$ |
| $\mathbf{1 4}$ | 3 | 33 | 0 | 10 | 0 | 0 | 53 | 0 | 6 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{1 3 9}$ |
| $\mathbf{1 5}$ | 7 | 0 | 0 | 2 | 0 | 0 | 10 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{2 6}$ |
| $\mathbf{1 6}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 7}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| Total | $\mathbf{1 3 5 3}$ | $\mathbf{1 2 7}$ | $\mathbf{9 9}$ | $\mathbf{3 9 8}$ | $\mathbf{4 8 4}$ | $\mathbf{2 1}$ | $\mathbf{1 0 3 9}$ | $\mathbf{7 0}$ | $\mathbf{2 9 3}$ | $\mathbf{8 8 4}$ | $\mathbf{5 0}$ | $\mathbf{0}$ | $\mathbf{6}$ | $\mathbf{1 3 8}$ | $\mathbf{5 5}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{5 0 1 7}$ |


| AM Heavy | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | $\mathbf{1 5}$ | $\mathbf{1 6}$ | $\mathbf{1 7}$ | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0 | 1 | 0 | 6 | 4 | 0 | 19 | 0 | 3 | 19 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | $\mathbf{5 4}$ |
| $\mathbf{2}$ | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | $\mathbf{5}$ |
| $\mathbf{3}$ | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{3}$ |
| $\mathbf{4}$ | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{1 2}$ |
| $\mathbf{5}$ | 3 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{1 2}$ |
| $\mathbf{6}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{7}$ | 11 | 1 | 2 | 4 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | $\mathbf{2 4}$ |
| $\mathbf{8}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{9}$ | 2 | 0 | 0 | 1 | 1 | 0 | 3 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{9}$ |
| $\mathbf{1 0}$ | 10 | 1 | 2 | 3 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | $\mathbf{2 2}$ |
| $\mathbf{1 1}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 2}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 3}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 4}$ | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{3}$ |
| $\mathbf{1 5}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 6}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 7}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| Total | $\mathbf{3 4}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{1 4}$ | $\mathbf{1 1}$ | $\mathbf{0}$ | $\mathbf{2 9}$ | $\mathbf{0}$ | $\mathbf{9}$ | $\mathbf{3 4}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{6}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{1 4 4}$ |

Simulation Model Background Traffic Demands - 2022 PM Peak

| PM Light | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | $\mathbf{1 5}$ | $\mathbf{1 6}$ | $\mathbf{1 7}$ | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0 | 59 | 0 | 73 | 234 | 8 | 479 | 0 | $\mathbf{9}$ | 408 | 0 | 0 | $\mathbf{4}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | 0 | 0 | $\mathbf{1 3 8 7}$ |
| $\mathbf{2}$ | 44 | 0 | 0 | 6 | 0 | 0 | 40 | 0 | 8 | 34 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | $\mathbf{1 6 4}$ |
| $\mathbf{3}$ | 16 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 3 | 14 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | $\mathbf{5 2}$ |
| $\mathbf{4}$ | 118 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 104 | 100 | 0 | 1 | 0 | 4 | 0 | 0 | $\mathbf{3 5 1}$ |
| $\mathbf{5}$ | 162 | 0 | 0 | 0 | 0 | 3 | 167 | 0 | 33 | 142 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{5 0 7}$ |
| $\mathbf{6}$ | 9 | 0 | 0 | 0 | 7 | 0 | 9 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{3 3}$ |
| $\mathbf{7}$ | 411 | 41 | 68 | 65 | 208 | 7 | 0 | 0 | 84 | 0 | 0 | 0 | 4 | 63 | 12 | 0 | 0 | $\mathbf{9 6 3}$ |
| $\mathbf{8}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{9}$ | 101 | 10 | 17 | 16 | 51 | 0 | 105 | 0 | 0 | 41 | 0 | 0 | 1 | 15 | 3 | 0 | 0 | $\mathbf{3 6 0}$ |
| $\mathbf{1 0}$ | 238 | 24 | 39 | 38 | 120 | 4 | 0 | 0 | 55 | 0 | 0 | 70 | 2 | 36 | 7 | 100 | 0 | $\mathbf{7 3 3}$ |
| $\mathbf{1 1}$ | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0 | $\mathbf{1 3 0}$ |
| $\mathbf{1 2}$ | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{4 0}$ |
| $\mathbf{1 3}$ | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{9}$ |
| $\mathbf{1 4}$ | 12 | 25 | 0 | 6 | 0 | 0 | 41 | 0 | 8 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{1 2 7}$ |
| $\mathbf{1 5}$ | 20 | 0 | 0 | 3 | 0 | 0 | 21 | 0 | 4 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{6}$ |
| $\mathbf{1 6}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 7}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| Total | $\mathbf{1 1 3 4}$ | $\mathbf{1 5 9}$ | $\mathbf{1 2 4}$ | $\mathbf{3 0 7}$ | $\mathbf{6 2 0}$ | $\mathbf{2 2}$ | $\mathbf{9 2 2}$ | $\mathbf{0}$ | $\mathbf{3 1 5}$ | $\mathbf{8 0 6}$ | $\mathbf{1 0 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2}$ | $\mathbf{1 6 1}$ | $\mathbf{4 0}$ | $\mathbf{1 0 0}$ | $\mathbf{0}$ | $\mathbf{4 9 2 2}$ |


| PM Heavy | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | $\mathbf{1 5}$ | $\mathbf{1 6}$ | $\mathbf{1 7}$ | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0 | 4 | 0 | 0 | 1 | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{1 7}$ |
| $\mathbf{2}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{3}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{4}$ | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{4}$ |
| $\mathbf{5}$ | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{9}$ |
| $\mathbf{6}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{7}$ | 11 | 0 | 4 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | $\mathbf{2 0}$ |
| $\mathbf{8}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{9}$ | 2 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{7}$ |
| $\mathbf{1 0}$ | 5 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{8}$ |
| $\mathbf{1 1}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 2}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 3}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 4}$ | $\mathbf{2}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{2}$ |
| $\mathbf{1 5}$ | $\mathbf{1}$ | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{3}$ |
| $\mathbf{1 6}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\mathbf{0}$ |
| $\mathbf{1 7}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ |
| Total | $\mathbf{2 6}$ | $\mathbf{4}$ | $\mathbf{7}$ | $\mathbf{1}$ | $\mathbf{4}$ | $\mathbf{0}$ | $\mathbf{1 2}$ | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{1 4}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{7 0}$ |

Simulation Model Traffic Demands - Development Traffic Only

| Original <br> AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| eid | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  | 18 | Total | eid | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | Total |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 0 | 0 | 145 | 181 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 181 | 181 |
| 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 27 | 34 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 34 | 34 |
| 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 11 | 14 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 14 |
| 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 40 | 50 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 0 | 0 | 50 |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 15 | 19 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 19 |
| 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 9 | 11 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 11 |
| 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 63 | 79 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 63 | 79 |
| 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 46 | 58 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 46 | 58 |
| 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 48 | 60 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | - | 0 | 48 | 60 |
| 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15 | 32 | 2 | 2 | 12 | 2 | 2 | 15 | 0 | 3 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 0 | 0 | 61 | 10 | '9 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 95 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18 | 128 | 6 | 9 | 49 | 8 | 7 | 60 | 0 | 12 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 160 | 8 | 11 | 0 | 0 | 0 | 60 | 0 | 15 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 317 |
| Total | 160 | 8 | 11 | 61 | 10 | 9 | 75 |  | 15 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 918 | Total | 160 | 8 | 11 | 61 | 10 | 9 | 75 | 0 | 15 | 63 | 0 | 0 | 0 | - | 119 | 0 | 0 | 387 | 918 |
| Original |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Revised |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| eid | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | Total | eid | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | Total |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 | 0 | 0 | 134 | 167 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 167 | 167 |
| 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 9 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 11 |
| 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 6 |
| 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | O | 7 | 0 | 0 | 29 | 36 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 0 | 0 | 0 | 36 |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 10 | 13 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 13 |
| 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 7 | 9 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 9 |
| 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | - | 53 | 66 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 53 | 66 |
| 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 30 | 37 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 30 | 37 |
| 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 43 | 54 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 43 | 54 |
| 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15 | 37 | 2 | 4 | 14 | 3 | 3 | 16 | 0 | 5 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 79 | 15 | 0 | 0 | 0 | $6^{\prime}$ | 14 | 16 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 115 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18 | 149 | 10 | 14 | 55 | 11 | 13 | 64 | 0 | 22 | 61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 320 | 18 | 186 | 12 | 18 | 0 | 0 | 0 | 64 | 0 | 27 | 76 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 383 |
| Total | 186 | 12 | 18 | 69 | 14 | 16 | 80 |  | 27 | 76 | 0 | 0 | 0 | 0 | 99 | 0 | 0 | 399 | 897 | Total | 186 | 12 | 18 | 69 | 14 | 16 | 80 | 0 | 27 | 76 |  | 0 | 0 | 0 | 89 | 0 | 0 | 310 | 897 |

# AnNexure B - Intersec tion Turn Volume Calbration 

GEH Values - All intersections


# Annexure C - Detailed Intersection Performance Metrics 

[^1]
## Scenario 1: Background Traffic - No Development



SC ENARIO 2: BACKG ROUND + DEVELOPMENT TRAFFIC - No
UPG RADES


SC ENARIO 3: BACKG ROUND + DEVELOPMENTTRAFFIC UPG RADE 1


SCENARIO 4: BACKGROUND TRAFFIC WITH DEVELOPMENT UPG RADE 2


SCenario 5: BACKG ROUND TRAFFIC WITH DEVELOPMENT-
UPG RADE 3


# Annexure D - Background Tkaffic Network Delays 

| Background Traffic (Sum of turn volume x delay) | Total Delays (sec) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM |  |  | PM |  |  | Both peaks |
| Network Scenario | Light | Heavy | Total | Light | Heavy | Total | All traffic |
| Scenario 1: Base existing network | 610316 | 18747 | 629062 | 524603 | 7970 | 532573 | 1161636 |
| Scenario 2: Base existing network with development | 780832 | 25094 | 805784 | 607906 | 11079 | 618853 | 1424637 |
| Scenario 3: Development + Upgrade 1 (lengthen slip-lane) | 670379 | 21410 | 691710 | 465789 | 9046 | 474789 | 1166498 |
| Scenario 4: Development + Upgrade 2 (slip lane +dual rights) | 595133 | 20335 | 615284 | 425934 | 7899 | 433747 | 1049031 |
| Scenario 5: Development +Upgrade 3 (slip lane + dual rights +re-alignment) | 595039 | 20273 | 615128 | 425706 | 7798 | 433418 | 1048546 |


| Background Traffic (Sum of turn volume x delay) | Total Delays (hours |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM |  |  | PM |  |  | Both peaks |
| Scenario | Light | Heavy | Total | Light | Heavy | Total | All traffic |
| Scenario 1: Base existing network | 170 | 5 | 175 | 146 | 2 | 148 | 323 |
| Scenario 2: Base existing netw ork with development | 217 | 7 | 224 | 169 | 3 | 172 | 396 |
| Scenario 3: Development +Upgrade 1 (lengthen slip-lane) | 186 | 6 | 192 | 129 | 3 | 132 | 324 |
| Scenario 4: Development + Upgrade 2 (slip lane +dual rights) | 165 | 6 | 171 | 118 | 2 | 120 | 291 |
| Scenario 5: Development +Upgrade 3 (slip lane +dual rights +re-alignment) | 165 | 6 | 171 | 118 | 2 | 120 | 291 |


| Background traffic \% Increase in delay vs Base | AM |  |  | PM |  |  | Both peaks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Network Scenario | Light | Heavy | Total | Light | Heavy | Total | All traffic |
| Scenario 2: Base existing network with development | 27.9\% | 33.9\% | 28.1\% | 15.9\% | 39.0\% | 16.2\% | 22.6\% |
| Scenario 3: Development +Upgrade 1 (lengthen slip-lane) | 9.8\% | 14.2\% | 10.0\% | -11.2\% | 13.5\% | -10.9\% | 0.4\% |
| Scenario 4: Development +Upgrade 2 (slip lane +dual rights) | -2.5\% | 8.5\% | -2.2\% | -18.8\% | -0.9\% | -18.6\% | -9.7\% |
| Scenario 5: Development +Upgrade 3 (slip lane + dual rights +re-alignment) | -2.5\% | 8.1\% | -2.2\% | -18.9\% | -2.2\% | -18.6\% | -9.7\% |

## Annexure E- Rnucane Road/ Delancey Street Signal Data



## AM Peak Signal Data



PM Peak Signal Data


## APPENDIX E- SIDRA OUTPUTS

## SITE LAYOUT

$\nabla$ Site: 101 [Delancey Street Site Access W/D 2024 AM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
4N


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Project: F:\Jobs\B19500\B19590\Design\Traffic\B19590 SIDRAS - Network.sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [Delancey Street Site Access W/D 2024 AM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn | $\begin{aligned} & \text { INF } \\ & \text { VOL؛ } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{gathered} \text { DEM } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \\ \hline \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { =UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 79 | 0.0 | 83 | 0.0 | 0.045 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.6 |
| 2 T1 | 329 | 4.0 | 346 | 4.0 | 0.182 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 3 R2 | 6 | 0.0 | 6 | 0.0 | 0.008 | 7.7 | LOSA | 0.0 | 0.2 | 0.54 | 0.65 | 0.54 | 51.0 |
| 3 u U | 1 | 0.0 | 1 | 0.0 | 0.008 | 11.7 | LOS B | 0.0 | 0.2 | 0.54 | 0.65 | 0.54 | 51.1 |
| Approach | 415 | 3.2 | 437 | 3.2 | 0.182 | 1.2 | NA | 0.0 | 0.2 | 0.01 | 0.12 | 0.01 | 58.4 |
| East: Arthur Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 0.0 | 7 | 0.0 | 0.024 | 8.6 | LOSA | 0.1 | 0.5 | 0.61 | 0.76 | 0.61 | 49.4 |
| 6 R2 | 3 | 0.0 | 3 | 0.0 | 0.024 | 18.0 | LOS C | 0.1 | 0.5 | 0.61 | 0.76 | 0.61 | 49.2 |
| Approach | 10 | 0.0 | 11 | 0.0 | 0.024 | 11.4 | LOS B | 0.1 | 0.5 | 0.61 | 0.76 | 0.61 | 49.3 |
| North: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.301 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 58.2 |
| 8 T1 | 545 | 2.0 | 574 | 2.0 | 0.301 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.8 |
| 9 R2 | 95 | 0.0 | 100 | 0.0 | 0.111 | 7.6 | LOS A | 0.4 | 3.1 | 0.48 | 0.70 | 0.48 | 51.5 |
| 9 u U | 1 | 0.0 | 1 | 0.0 | 0.111 | 9.3 | LOSA | 0.4 | 3.1 | 0.48 | 0.70 | 0.48 | 51.6 |
| Approach | 643 | 1.7 | 677 | 1.7 | 0.301 | 1.2 | NA | 0.4 | 3.1 | 0.07 | 0.11 | 0.07 | 58.4 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 126 | 0.0 | 133 | 0.0 | 0.143 | 7.3 | LOSA | 0.5 | 3.7 | 0.42 | 0.67 | 0.42 | 52.3 |
| Approach | 126 | 0.0 | 133 | 0.0 | 0.143 | 7.3 | LOSA | 0.5 | 3.7 | 0.42 | 0.67 | 0.42 | 52.3 |
| All Vehicles | 1194 | 2.0 | 1257 | 2.0 | 0.301 | 2.0 | NA | 0.5 | 3.7 | 0.09 | 0.18 | 0.09 | 57.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [Delancey Street Site Access W/D 2024 PM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { JT } \\ \text { UES } \\ \text { HV ] } \\ \% \end{gathered}$ | $\begin{aligned} & \text { DEM } \\ & \text { FLOO } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B/ } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \\ \hline \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 59 | 4.0 | 62 | 4.0 | 0.034 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.4 |
| 2 T1 | 322 | 0.0 | 339 | 0.0 | 0.174 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 3 R 2 | 9 | 0.0 | 9 | 0.0 | 0.010 | 6.9 | LOS A | 0.0 | 0.3 | 0.46 | 0.61 | 0.46 | 51.8 |
| 3 u U | 1 | 0.0 | 1 | 0.0 | 0.010 | 9.8 | LOSA | 0.0 | 0.3 | 0.46 | 0.61 | 0.46 | 51.9 |
| Approach | 391 | 0.6 | 412 | 0.6 | 0.174 | 1.1 | NA | 0.0 | 0.3 | 0.01 | 0.10 | 0.01 | 58.6 |
| East: Arthur Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 6 | 0.0 | 6 | 0.0 | 0.014 | 7.5 | LOS A | 0.0 | 0.3 | 0.50 | 0.67 | 0.50 | 50.9 |
| 6 R2 | 2 | 0.0 | 2 | 0.0 | 0.014 | 14.6 | LOS B | 0.0 | 0.3 | 0.50 | 0.67 | 0.50 | 50.6 |
| Approach | 8 | 0.0 | 8 | 0.0 | 0.014 | 9.3 | LOS A | 0.0 | 0.3 | 0.50 | 0.67 | 0.50 | 50.8 |
| North: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 3 | 1.0 | 3 | 1.0 | 0.225 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 58.2 |
| 8 T1 | 408 | 1.0 | 429 | 1.0 | 0.225 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.8 |
| 9 R2 | 69 | 0.0 | 73 | 0.0 | 0.078 | 7.3 | LOS A | 0.3 | 2.1 | 0.45 | 0.67 | 0.45 | 51.7 |
| 9 u U | 1 | 0.0 | 1 | 0.0 | 0.078 | 9.1 | LOSA | 0.3 | 2.1 | 0.45 | 0.67 | 0.45 | 51.8 |
| Approach | 481 | 0.9 | 506 | 0.9 | 0.225 | 1.2 | NA | 0.3 | 2.1 | 0.07 | 0.10 | 0.07 | 58.5 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 176 | 2.0 | 185 | 2.0 | 0.199 | 7.4 | LOS A | 0.8 | 5.5 | 0.43 | 0.68 | 0.43 | 52.2 |
| Approach | 176 | 2.0 | 185 | 2.0 | 0.199 | 7.4 | LOS A | 0.8 | 5.5 | 0.43 | 0.68 | 0.43 | 52.2 |
| All <br> Vehicles | 1056 | 0.9 | 1112 | 0.9 | 0.225 | 2.2 | NA | 0.8 | 5.5 | 0.11 | 0.20 | 0.11 | 57.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [Delancey Street Site Access W/D 2034 AM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 79 | 0.0 | 83 | 0.0 | 0.045 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.6 |
| 2 T1 | 440 | 4.0 | 463 | 4.0 | 0.244 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 3 R 2 | 7 | 0.0 | 7 | 0.0 | 0.011 | 8.2 | LOS A | 0.0 | 0.3 | 0.57 | 0.68 | 0.57 | 50.7 |
| 3 u U | 1 | 0.0 | 1 | 0.0 | 0.011 | 12.7 | LOS B | 0.0 | 0.3 | 0.57 | 0.68 | 0.57 | 50.8 |
| Approach | 527 | 3.3 | 555 | 3.3 | 0.244 | 1.0 | NA | 0.0 | 0.3 | 0.01 | 0.10 | 0.01 | 58.7 |
| East: Arthur Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 8 | 0.0 | 8 | 0.0 | 0.037 | 9.2 | LOS A | 0.1 | 0.8 | 0.69 | 0.82 | 0.69 | 47.7 |
| 6 R2 | 4 | 0.0 | 4 | 0.0 | 0.037 | 23.6 | LOS C | 0.1 | 0.8 | 0.69 | 0.82 | 0.69 | 47.5 |
| Approach | 12 | 0.0 | 13 | 0.0 | 0.037 | 14.0 | LOS B | 0.1 | 0.8 | 0.69 | 0.82 | 0.69 | 47.6 |
| North: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 3 | 0.0 | 3 | 0.0 | 0.335 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 58.2 |
| 8 T1 | 605 | 2.0 | 637 | 2.0 | 0.335 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.8 |
| 9 R2 | 95 | 0.0 | 100 | 0.0 | 0.129 | 8.5 | LOS A | 0.5 | 3.5 | 0.54 | 0.77 | 0.54 | 50.9 |
| 9 u U | 1 | 0.0 | 1 | 0.0 | 0.129 | 10.7 | LOS B | 0.5 | 3.5 | 0.54 | 0.77 | 0.54 | 50.9 |
| Approach | 704 | 1.7 | 741 | 1.7 | 0.335 | 1.3 | NA | 0.5 | 3.5 | 0.07 | 0.11 | 0.07 | 58.4 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 126 | 0.0 | 133 | 0.0 | 0.166 | 8.2 | LOS A | 0.6 | 4.2 | 0.49 | 0.74 | 0.49 | 51.6 |
| Approach | 126 | 0.0 | 133 | 0.0 | 0.166 | 8.2 | LOS A | 0.6 | 4.2 | 0.49 | 0.74 | 0.49 | 51.6 |
| All <br> Vehicles | 1369 | 2.2 | 1441 | 2.2 | 0.335 | 1.9 | NA | 0.6 | 4.2 | 0.09 | 0.17 | 0.09 | 57.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [Delancey Street Site Access W/D 2034 PM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { vOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 59 | 4.0 | 62 | 4.0 | 0.034 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.4 |
| 2 T1 | 359 | 0.0 | 378 | 0.0 | 0.194 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 3 R 2 | 10 | 0.0 | 11 | 0.0 | 0.011 | 7.1 | LOSA | 0.0 | 0.3 | 0.48 | 0.62 | 0.48 | 51.7 |
| 3 u U | 1 | 0.0 | 1 | 0.0 | 0.011 | 10.2 | LOS B | 0.0 | 0.3 | 0.48 | 0.62 | 0.48 | 51.7 |
| Approach | 429 | 0.6 | 452 | 0.6 | 0.194 | 1.0 | NA | 0.0 | 0.3 | 0.01 | 0.10 | 0.01 | 58.7 |
| East: Arthur Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 0.0 | 7 | 0.0 | 0.017 | 7.7 | LOS A | 0.1 | 0.4 | 0.52 | 0.68 | 0.52 | 50.6 |
| 6 R2 | 2 | 0.0 | 2 | 0.0 | 0.017 | 16.2 | LOS C | 0.1 | 0.4 | 0.52 | 0.68 | 0.52 | 50.4 |
| Approach | 9 | 0.0 | 9 | 0.0 | 0.017 | 9.6 | LOS A | 0.1 | 0.4 | 0.52 | 0.68 | 0.52 | 50.6 |
| North: Delancey Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 4 | 1.0 | 4 | 1.0 | 0.245 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 58.2 |
| 8 T1 | 444 | 1.0 | 467 | 1.0 | 0.245 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 59.8 |
| 9 R2 | 69 | 0.0 | 73 | 0.0 | 0.082 | 7.6 | LOS A | 0.3 | 2.2 | 0.47 | 0.69 | 0.47 | 51.5 |
| 9 u U | 1 | 0.0 | 1 | 0.0 | 0.082 | 9.5 | LOSA | 0.3 | 2.2 | 0.47 | 0.69 | 0.47 | 51.6 |
| Approach | 518 | 0.9 | 545 | 0.9 | 0.245 | 1.1 | NA | 0.3 | 2.2 | 0.06 | 0.10 | 0.06 | 58.5 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 176 | 2.0 | 185 | 2.0 | 0.208 | 7.6 | LOS A | 0.8 | 5.7 | 0.46 | 0.71 | 0.46 | 52.0 |
| Approach | 176 | 2.0 | 185 | 2.0 | 0.208 | 7.6 | LOS A | 0.8 | 5.7 | 0.46 | 0.71 | 0.46 | 52.0 |
| All <br> Vehicles | 1132 | 0.9 | 1192 | 0.9 | 0.245 | 2.2 | NA | 0.8 | 5.7 | 0.11 | 0.20 | 0.11 | 57.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

## Site: 101 [Finucane Road Site Access W/D 2024 AM (Site

 Folder: Access SIDRAS)]New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


Finucane Road

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## MOVEMENT SUMMARY

Site: 101 [Finucane Road Site Access W/D 2024 AM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE <br> [ Veh. Dist] veh m |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 1548 | 2.0 | 1629 | 2.0 | 0.595 | 6.9 | LOS A | 17.7 | 126.0 | 0.54 | 0.50 | 0.54 | 53.9 |
| 6 R2 | 142 | 0.0 | 149 | 0.0 | * 0.604 | 47.1 | LOS D | 6.5 | 45.4 | 0.99 | 0.81 | 1.01 | 33.3 |
| Approach | 1690 | 1.8 | 1779 | 1.8 | 0.604 | 10.3 | LOS B | 17.7 | 126.0 | 0.58 | 0.52 | 0.58 | 51.2 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 133 | 0.0 | 140 | 0.0 | 0.212 | 27.3 | LOS C | 4.3 | 30.0 | 0.74 | 0.75 | 0.74 | 40.7 |
| 9 R2 | 142 | 0.0 | 149 | 0.0 | * 0.517 | 44.5 | LOS D | 6.2 | 43.7 | 0.97 | 0.80 | 0.97 | 34.2 |
| Approach | 275 | 0.0 | 289 | 0.0 | 0.517 | 36.2 | LOS D | 6.2 | 43.7 | 0.85 | 0.78 | 0.85 | 37.0 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 230 | 0.0 | 242 | 0.0 | 0.178 | 9.5 | LOS A | 3.2 | 22.4 | 0.33 | 0.65 | 0.33 | 51.4 |
| 11 T1 | 1124 | 4.0 | 1183 | 4.0 | * 0.620 | 16.7 | LOS B | 18.9 | 136.5 | 0.76 | 0.68 | 0.76 | 47.0 |
| Approach | 1354 | 3.3 | 1425 | 3.3 | 0.620 | 15.5 | LOS B | 18.9 | 136.5 | 0.69 | 0.68 | 0.69 | 47.7 |
| All Vehicles | 3319 | 2.3 | 3494 | 2.3 | 0.620 | 14.6 | LOS B | 18.9 | 136.5 | 0.65 | 0.61 | 0.65 | 48.2 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  | ACK OF <br> Dist ] | Prop. EffectiveQue $\begin{aligned} & \text { Stop } \\ & \text { Rate }\end{aligned}$ |  | Travel Time | Travel Aver. Dist. Speed m m/sec |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 208.9 | 220.5 | 1.06 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.8 | 213.9 | 1.05 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P4BSlip/ Bypass | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 196.4 | 204.3 | 1.04 |
| All <br> Pedestrians | 150 | 158 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.1 | 212.9 | 1.05 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [Finucane Road Site Access W/D 2024 AM (Site Folder: Access SIDRAS)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase A
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

| Phase Timing Summary |
| :--- |
| Phase A B C <br> Phase Change Time (sec) 0 18 70 <br> Green Time (sec) 12 46 14 <br> Phase Time (sec) 18 52 20 <br> Phase Split $20 \%$ $58 \%$ $22 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Oermitted/Opposed
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## MOVEMENT SUMMARY

Site: 101 [Finucane Road Site Access W/D 2024 PM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. Aver. No. Speed Cycles km/h |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 1441 | 2.0 | 1517 | 2.0 | 0.601 | 9.4 | LOS A | 18.7 | 133.3 | 0.62 | 0.56 | 0.62 | 52.0 |
| 6 R2 | 124 | 0.0 | 131 | 0.0 | * 0.633 | 49.4 | LOS D | 5.8 | 40.9 | 1.00 | 0.82 | 1.06 | 32.6 |
| Approach | 1565 | 1.8 | 1647 | 1.8 | 0.633 | 12.6 | LOS B | 18.7 | 133.3 | 0.65 | 0.58 | 0.65 | 49.6 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 171 | 0.0 | 180 | 0.0 | 0.249 | 25.5 | LOS C | 5.3 | 37.4 | 0.72 | 0.76 | 0.72 | 41.5 |
| 9 R2 | 228 | 0.0 | 240 | 0.0 | * 0.612 | 41.1 | LOS D | 9.8 | 68.6 | 0.96 | 0.82 | 0.96 | 35.3 |
| Approach | 399 | 0.0 | 420 | 0.0 | 0.612 | 34.4 | LOS C | 9.8 | 68.6 | 0.85 | 0.79 | 0.85 | 37.7 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 190 | 0.0 | 200 | 0.0 | 0.143 | 8.8 | LOS A | 2.4 | 16.5 | 0.29 | 0.64 | 0.29 | 51.9 |
| 11 T1 | 1083 | 1.0 | 1140 | 1.0 | * 0.623 | 18.7 | LOS B | 18.8 | 132.6 | 0.80 | 0.71 | 0.80 | 45.9 |
| Approach | 1273 | 0.9 | 1340 | 0.9 | 0.623 | 17.2 | LOS B | 18.8 | 132.6 | 0.72 | 0.70 | 0.72 | 46.7 |
| All Vehicles | 3237 | 1.2 | 3407 | 1.2 | 0.633 | 17.1 | LOS B | 18.8 | 133.3 | 0.70 | 0.65 | 0.70 | 46.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay <br> sec |  | Level of AVERAGE BACK OF Service QUEUE |  | Prop. EffectiveQue $\begin{aligned} & \text { Stop } \\ & \\ & \\ & \\ & \text { Rate }\end{aligned}$ |  | Travel Time sec | Travel Aver. Dist. Speed $\mathrm{mm} / \mathrm{sec}$ |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 208.9 | 220.5 | 1.06 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.8 | 213.9 | 1.05 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P4BSlip/ <br> Bypass | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 196.4 | 204.3 | 1.04 |
| All <br> Pedestrians | 150 | 158 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.1 | 212.9 | 1.05 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [Finucane Road Site Access W/D 2024 PM (Site Folder: Access SIDRAS)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase A
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

| Phase Timing Summary |
| :--- |
| Phase A B C <br> Phase Change Time (sec) 0 16 65 <br> Green Time (sec) 10 43 19 <br> Phase Time (sec) 16 49 25 <br> Phase Split $18 \%$ $54 \%$ $28 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Oermitted/Opposed
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## MOVEMENT SUMMARY

Site: 101 [Finucane Road Site Access W/D 2034 AM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. Aver. No. Speed Cycles km/h |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 1656 | 2.0 | 1743 | 2.0 | 0.637 | 7.3 | LOS A | 20.0 | 142.1 | 0.57 | 0.53 | 0.57 | 53.6 |
| 6 R2 | 142 | 0.0 | 149 | 0.0 | * 0.659 | 48.9 | LOS D | 6.7 | 46.7 | 1.00 | 0.83 | 1.07 | 32.8 |
| Approach | 1798 | 1.8 | 1893 | 1.8 | 0.659 | 10.6 | LOS B | 20.0 | 142.1 | 0.61 | 0.55 | 0.61 | 51.0 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 133 | 0.0 | 140 | 0.0 | 0.219 | 28.1 | LOS C | 4.4 | 30.5 | 0.75 | 0.75 | 0.75 | 40.3 |
| 9 R2 | 184 | 0.0 | 194 | 0.0 | * 0.670 | 46.4 | LOS D | 8.5 | 59.2 | 0.99 | 0.84 | 1.05 | 33.6 |
| Approach | 317 | 0.0 | 334 | 0.0 | 0.670 | 38.7 | LOS D | 8.5 | 59.2 | 0.89 | 0.80 | 0.93 | 36.1 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 230 | 0.0 | 242 | 0.0 | 0.175 | 9.2 | LOS A | 3.1 | 21.4 | 0.31 | 0.65 | 0.31 | 51.6 |
| 11 T1 | 1287 | 4.0 | 1355 | 4.0 | * 0.713 | 17.1 | LOS B | 23.6 | 170.8 | 0.80 | 0.72 | 0.80 | 46.8 |
| Approach | 1517 | 3.4 | 1597 | 3.4 | 0.713 | 15.9 | LOS B | 23.6 | 170.8 | 0.73 | 0.71 | 0.73 | 47.5 |
| All Vehicles | 3632 | 2.3 | 3823 | 2.3 | 0.713 | 15.3 | LOS B | 23.6 | 170.8 | 0.68 | 0.64 | 0.69 | 47.8 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  | ACK OF <br> Dist ] | Prop. EffectiveQue $\begin{aligned} & \text { Stop } \\ & \text { Rate }\end{aligned}$ |  | Travel Time | Travel Aver. Dist. Speed m m/sec |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 208.9 | 220.5 | 1.06 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.8 | 213.9 | 1.05 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P4BSlip/ Bypass | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 196.4 | 204.3 | 1.04 |
| All <br> Pedestrians | 150 | 158 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.1 | 212.9 | 1.05 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [Finucane Road Site Access W/D 2034 AM (Site Folder: Access SIDRAS)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase A
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

| Phase Timing Summary |  |  |  |
| :---: | :---: | :---: | :---: |
| Phase | A | B | C |
| Phase Change Time (sec) | 0 | 17 | 70 |
| Green Time (sec) | 11 | 47 | 14 |
| Phase Time (sec) | 17 | 53 | 20 |
| Phase Split | 19\% | 59\% | 22\% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Oermitted/Opposed
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## MOVEMENT SUMMARY

Site: 101 [Finucane Road Site Access W/D 2034 PM (Site
Folder: Access SIDRAS)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. Aver. No. Speed Cycles km/h |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 1589 | 2.0 | 1673 | 2.0 | 0.641 | 8.8 | LOS A | 20.7 | 147.3 | 0.62 | 0.57 | 0.62 | 52.4 |
| 6 R2 | 124 | 0.0 | 131 | 0.0 | * 0.633 | 49.4 | LOS D | 5.8 | 40.9 | 1.00 | 0.82 | 1.06 | 32.6 |
| Approach | 1713 | 1.9 | 1803 | 1.9 | 0.641 | 11.7 | LOS B | 20.7 | 147.3 | 0.65 | 0.59 | 0.65 | 50.2 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 171 | 0.0 | 180 | 0.0 | 0.264 | 27.1 | LOS C | 5.5 | 38.8 | 0.74 | 0.76 | 0.74 | 40.8 |
| 9 R2 | 228 | 0.0 | 240 | 0.0 | * 0.684 | 44.1 | LOS D | 10.3 | 72.1 | 0.99 | 0.85 | 1.04 | 34.3 |
| Approach | 399 | 0.0 | 420 | 0.0 | 0.684 | 36.8 | LOS D | 10.3 | 72.1 | 0.88 | 0.81 | 0.91 | 36.8 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 190 | 0.0 | 200 | 0.0 | 0.143 | 8.8 | LOS A | 2.4 | 16.5 | 0.29 | 0.64 | 0.29 | 51.9 |
| 11 T1 | 1239 | 1.0 | 1304 | 1.0 | * 0.695 | 18.2 | LOS B | 22.6 | 159.6 | 0.81 | 0.73 | 0.81 | 46.2 |
| Approach | 1429 | 0.9 | 1504 | 0.9 | 0.695 | 17.0 | LOS B | 22.6 | 159.6 | 0.74 | 0.72 | 0.74 | 46.9 |
| All Vehicles | 3541 | 1.2 | 3727 | 1.2 | 0.695 | 16.7 | LOS B | 22.6 | 159.6 | 0.71 | 0.66 | 0.72 | 46.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \\ & \text { IDossing } \end{aligned}$ | Input Vol. <br> $\mathrm{ped} / \mathrm{h}$ | Dem. Flow <br> ped/h | Aver. Delay $\qquad$ sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que $\begin{aligned} & \text { Stop } \\ & \text { Rate }\end{aligned}$ |  | Travel Time <br> sec | Travel Aver. Dist. Speed$\qquad$ |  |
| East: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 208.9 | 220.5 | 1.06 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.8 | 213.9 | 1.05 |
| West: Finucane Road |  |  |  |  |  |  |  |  |  |  |  |
| P4BSlip/ Bypass | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 196.4 | 204.3 | 1.04 |
| All <br> Pedestrians | 150 | 158 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 203.1 | 212.9 | 1.05 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [Finucane Road Site Access W/D 2034 PM (Site Folder: Access SIDRAS)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase A
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

| Phase Timing Summary |
| :--- |
| Phase A B C <br> Phase Change Time (sec) 0 16 67 <br> Green Time (sec) 10 45 17 <br> Phase Time (sec) 16 51 23 <br> Phase Split $18 \%$ $57 \%$ $26 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Oermitted/Opposed
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped



[^0]:    Carficatons ano olscamers
     Hi Phu
    

[^1]:    The following tables contain the modelled turn volumes (background plus development traffic) and the associated delays for each turn movement. The approach and intersection delays are the weighted average of the respective turn delays.

